

**The Development of an Analytical Model for the
KODAK DIGITAL SCIENCE™ Color Infrared Cameras
and Its Aerial Imaging Applications**

**Imaging Science MS Project
Todd Birdsall
Summer, 1997**

Acknowledgments:

I would like to acknowledge and thank the following people for their support on this project :

Dr. John Schott, Professor, Director, Digital Image & Remote Sensing Laboratory, RIT
- Overall project advisor

Mr. Rolando Raqueño, Associate Scientist, RIT
- Weekly technical direction and support

Mr. John Newman, Senior System Engineer, Eastman Kodak Company
- Color science technical advice

Mr. Mark Shrader, Senior Development Engineer, Eastman Kodak Company
- Camera software driver technical advice

Dedication:

This paper is dedicated to my loving wife, Debbie, and to my two great kids, Holly and Troy. My family has inspired and supported me throughout my academic career at RIT.

Abstract:

The new KODAK DIGITAL SCIENCE™ Color Infrared Cameras provide an affordable, high-resolution digital imaging solution for many low-altitude remote sensing applications. These remote sensing applications span forest management, law enforcement, environmental monitoring and agriculture crop analysis. This paper describes the technical aspects of the color infrared (CIR) cameras, and an analytical model of the cameras in aerial imaging scenarios. The model is based on physical attributes of the imaging chain and incorporates Modtran atmospheric data, measured ground target reflectance data, predicted aircraft motion, and measured/computed camera characteristics. It is capable of predicting both radiometric and image quality performance of a complete aerial image chain. Output data is in terms of 8-bit digital counts for the radiometric computations and ground resolving distance (GRD) for image quality analysis. normalized difference vegetation index (NDVI), for agriculture analysis, is also computed. The model is flexible and robust enough to predict over system performance in real life imaging scenarios or to be used as a design tool for camera optimization.

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1.0 Background

1.1 CIR Camera Overview

The utilization of traditional infrared film photography for various applications has been well documented in many publications. Key current applications include forest management, law enforcement, environmental monitoring and agriculture crop analysis.

The KODAK DIGITAL SCIENCE™ Color Infrared Digital Cameras provide the benefits of infrared film along with a multitude of digital imaging benefits. Kodak currently offers two models of the infrared cameras. The KODAK DIGITAL SCIENCE™ 420 Color Infrared Camera and KODAK DIGITAL SCIENCE™ 460 Color Infrared Camera. The major difference between the two camera models is the size of the CCD imager. The 420 model has a 1.5 million pixel array incorporated into it while the 460 model utilizes a 6 million pixel imager.

The CIR digital cameras are not intended to replace the current 9 inch x 9 inch aerial infrared mapping films. The mapping films have superior resolution and orders of magnitude more area coverage capabilities than the current CIR cameras. For example, if a 9 inch x 9 inch piece of film was scanned at 9 μm x 9 μm pixel pitch with a dynamic range of 8 bits per color, the resulting image file size would be 1.9 GB. This is over 100 times larger than the image files from the 460 CIR camera. The 460 model produces a final file size of 18 MB per image.

The CIR camera and the infrared film essentially have the same spectral response. The spectral response of the CIR camera is slightly broader than the infrared film. The camera, with its silicon CCD, is sensitive from 400 nanometers (nm) to 1000 nm. The film's sensitivity falls between 400-900 nm. The 100 nm difference from 900 nm to 1000 nm is trivial for most aerial applications because of the H₂O absorption band in the atmosphere of between 900 nm and 1000 nm.

The benefits of the CIR cameras lies in their ability to produce reliable, repeatable images in a fraction of the time it would take to get the same results from traditional film. The output images from the digital camera are essentially instant. Some aerial photographers use the camera in conjunction with an on-board computer and view the imagery in-flight. The imagery from the CIR cameras are very consistent under the same capture conditions. This fact gives rise to the possibility of using the cameras as a radiometer for some remote sensing applications. In comparison, film radiometry is very difficult because of its roll-to-roll sensitometric variations.

A major revolution in remote sensing imagery is taking place. Over the next few years, electro-optical (E-O), multispectral high-resolution, commercial satellite imagery will be readily available to everyone. Currently, there is multispectral (MS) imagery available from satellite systems like Landsat and Spot. These systems produce MS imagery at 30 meter and 10 meter ground sample distance (GSD), respectively. Soon to be launched are high-resolution satellite systems like Space Imaging and EarthWatch. Both systems will provide MS imagery at 4 meter GSD.

There is no question that the new imaging satellites will compete with the aerial photography industry. The questions that still remains is how much, and how fast? Satellites have inherent system constraints that impact their ability to capture acceptable results. Some of the system constraints that must be considered include resolution, cloud-covered targets, and target revisit time. The new breed of commercial satellites will be resolution limited, by law, to 1 meter panchromatic GSD and 4 meter MS GSD or less. With this GSD constraint, objects smaller than 2 meters will not be resolvable. The new commercial E-O satellites have two other major limitations. First, they cannot image targets that are cloud covered. This means land mass that is primarily cloud covered will not be imaged by satellites very often. Secondly, satellites fly in specific elliptical orbits, which affects their ability to revisit specific targets at a specific resolution periodically. Targets will only be in view for a very short time, and only once a month or longer, until more satellites are deployed.

Aerial photography is not limited by these satellite constraints. Aircraft can achieve greater than 1 meter GSD. Depending on the urgency of the imagery, aircraft can fly under clouds and acquire images. Aircraft can fly over a target at the same resolution as necessary. This is a requirement for such applications as emergency rescue operations and some crop analysis projects.

1.2 Model Overview

The need for accurately predicting overall system performance is a must for today's imaging systems. No performance prediction model of the CIR camera exists. Also, there is no CIR camera optimization tool addressing the entire image chain. This paper presents an analytical CIR camera model that embodies the entire aerial imaging chain.

The focus of this paper is a detailed description of the model. In section 2, the approach of the model is presented. Section 3 is a technical description of all of the imaging chain components of the model and their interactions. Section 4 provides results of a modeling case study. The case study utilized three temporal states of wheat to show the robustness of the model and the CIR camera. Also, output imagery of the camera is presented in empirical form. In section 5, conclusions, summaries and possible follow-on work is presented.

2.0 Approach

A systems approach to model the physical attributes of each part of the imaging chain has been adopted. The atmosphere, ground target, aircraft, CIR camera, and digital image processing (Adobe Photoshop plug-in drivers) make up the major components of the imaging chain in the model. The model consists of two separate spreadsheets. One spreadsheet predicts the 8-bit digital count output of the camera's radiometric response in the imaging chain. The second spreadsheet estimates image quality of the camera's output in the imaging chain. In order to make the model as accurate as possible, measured data was used when available. Such data includes target reflectance data, filter and lens performance data, and CCD responsivity data. The details of the measured data are presented in section 3.

The radiometric model uses only reflected energy (no self-emission energy) throughout the imaging chain. Figure 1 depicts the solar energy path, as modeled in the radiometric model. Solar-ray "A" represents the exoatmospheric spectral irradiance. Solar-ray "B" represents the downwelled solar radiance. Solar-ray "C" represents the upwelled solar radiance¹³.

The atmosphere is modeled by incorporating Modtran data into it. The model assumes a lambertian (no angular dependence) ground target and no spectral shift with a change in solar zenith angle. Output of the radiometric analysis is in terms of 8-bit digital counts for a particular pixel .

SOLAR ENERGY PATH

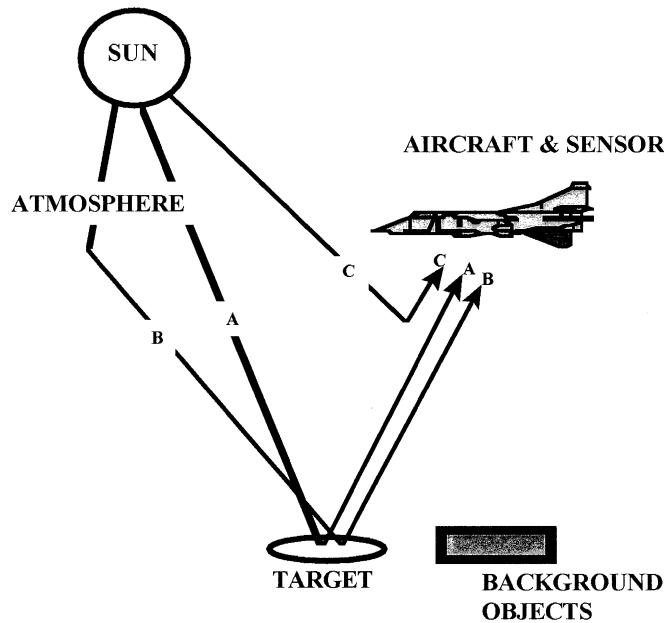


Figure 1: Solar Energy Path in the Imaging Chain

The image quality model is based on threshold modulation analysis (TMA)⁹. TMA compares the input or available modulation (ITM) to the required or needed modulation (TM) to predict an overall performance. The comparison between the input and required modulations can take place at any part in the imaging chain. The image quality model compares the two modulations at the focal plane. The image quality model uses data computed from the radiometric model (signal electrons, noise electrons, and the NDVI) as input for the noise modulation and target contrast calculations. The model assumes a linear system such that individual modulation transfer functions (MTF) can be cascaded together to predict overall input and required ITM. Both in-track and cross-track MTFs are computed and analyzed. The final output of the image quality portion is ground resolving distance (GRD) for a specific colored pixel.

3.0 Technical Description

3.1 Color Infrared Camera

The color infrared cameras are derivatives of the KODAK PROFESSIONAL DCS Digital Cameras. Both the CIR and the Professional DCS cameras have silicon CCDs. To achieve three-channel information, the CCDs utilize a color filter array (CFA), “Bayer pattern” design^{1,3,8}. The CFA protocol is 25% of the total pixels are red, 50% are green, and 25% are blue. Like most silicon CCDs, the Kodak cameras’ CCDs are responsive from 400 nm to 1000 nm. The quantum efficiency (QE) curve of the 460 model’s CCD is shown below in Figure 2.⁶

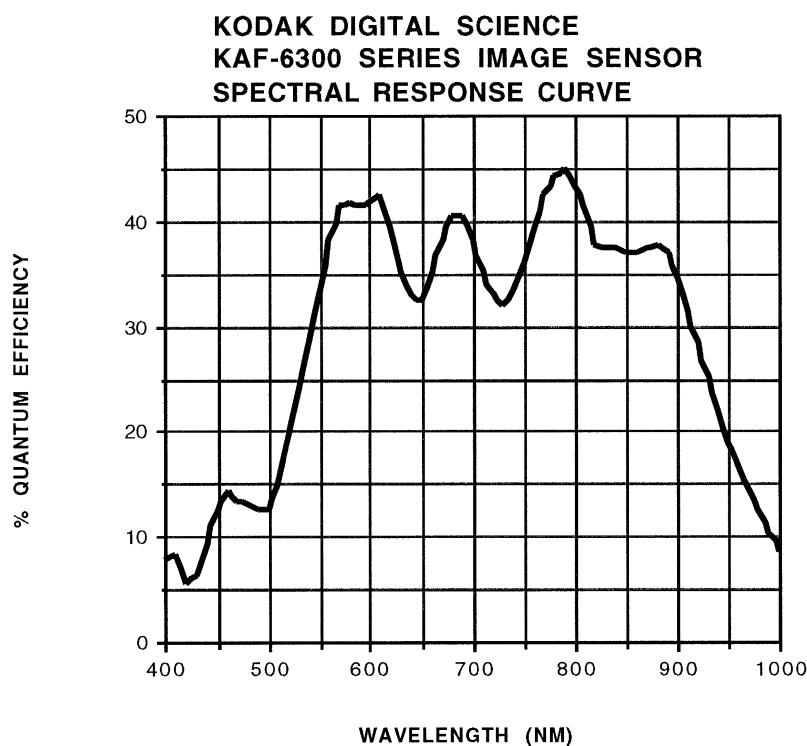


Figure 2: CCD Spectral Response Plot

The QE for the 420 camera is essentially the same. The Bayer pattern CFA of the CCD for the 460 camera is shown below in Figure 3.⁸

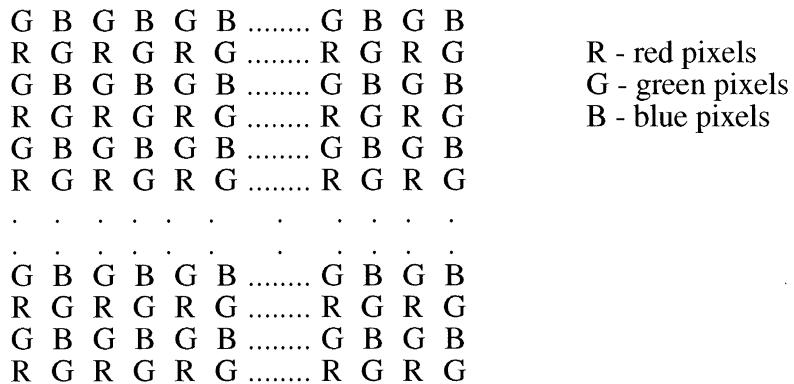


Figure 3: Color Filter Array (CFA) made by KODAK

As shown in Figure 4, the unique dye layers of the CFA are not only transmissive in their respective color-band, but also in the near-infrared region. It is this transmissive fact that makes the CIR version of the cameras possible. Note these curves are normalized to 80% peak in the model.

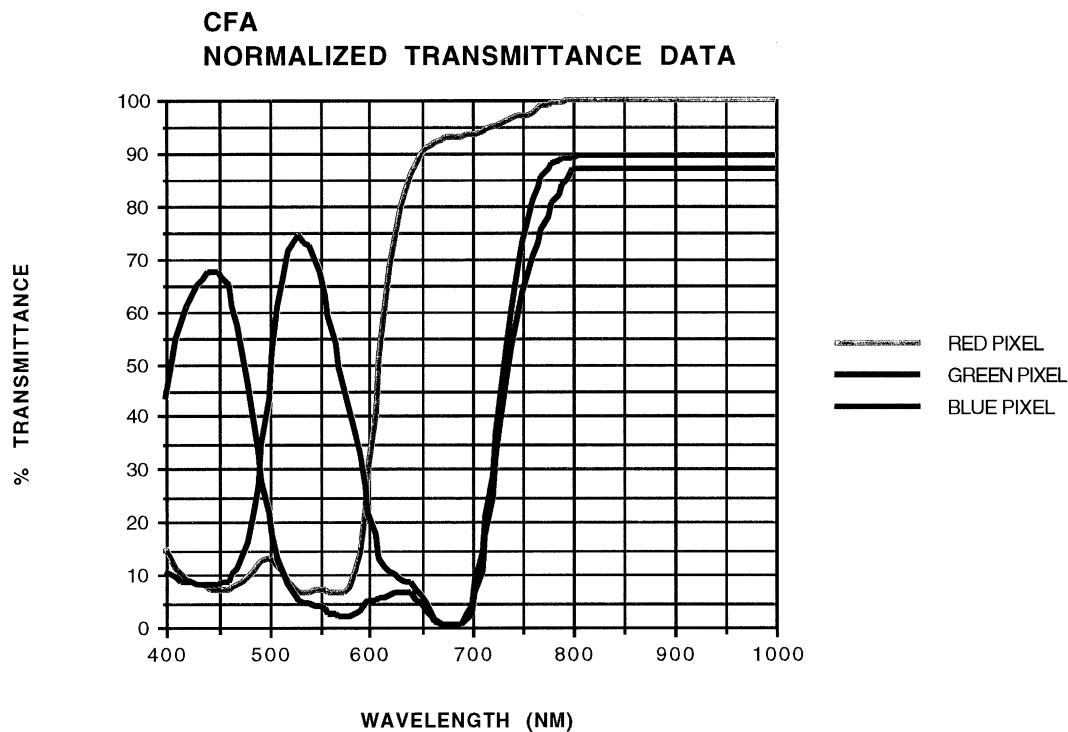


Figure 4: Color Filter Array Normalized Transmittance Plot

Color Infrared Capture

The diagram below illustrates the entire color infrared capturing process.

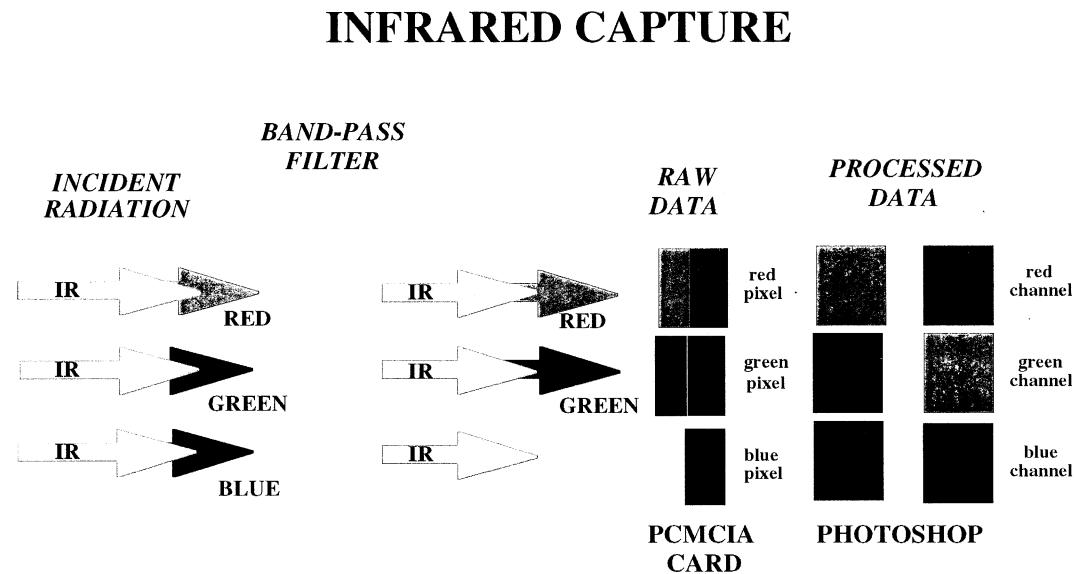


Figure 5: Infrared Capture

In order to use the CFA to capture near-infrared radiation, three major differences between the CIR and the generic Professional DCS cameras are required. These differences include the cover-glass on the charge coupled device (CCD), the lens band-pass filters, and image-processing software used to view the images. The CIR cameras are manufactured with a so-called clear cover glass, which allows infrared radiation to penetrate to the collecting portion of the CCD. The Professional DCS camera versions have IR attenuating cover glass on it.

The CIR cameras come with two distinct band-pass filters that screw on the front of the Nikon lenses.⁶ The 650BP300 is used for near-infrared imaging and has a band-pass from 500 nm to 800 nm. The VIS filter is used to acquire natural color images from the CIR camera. Figure 6 shows the measured transmittance of the two CIR camera filters.

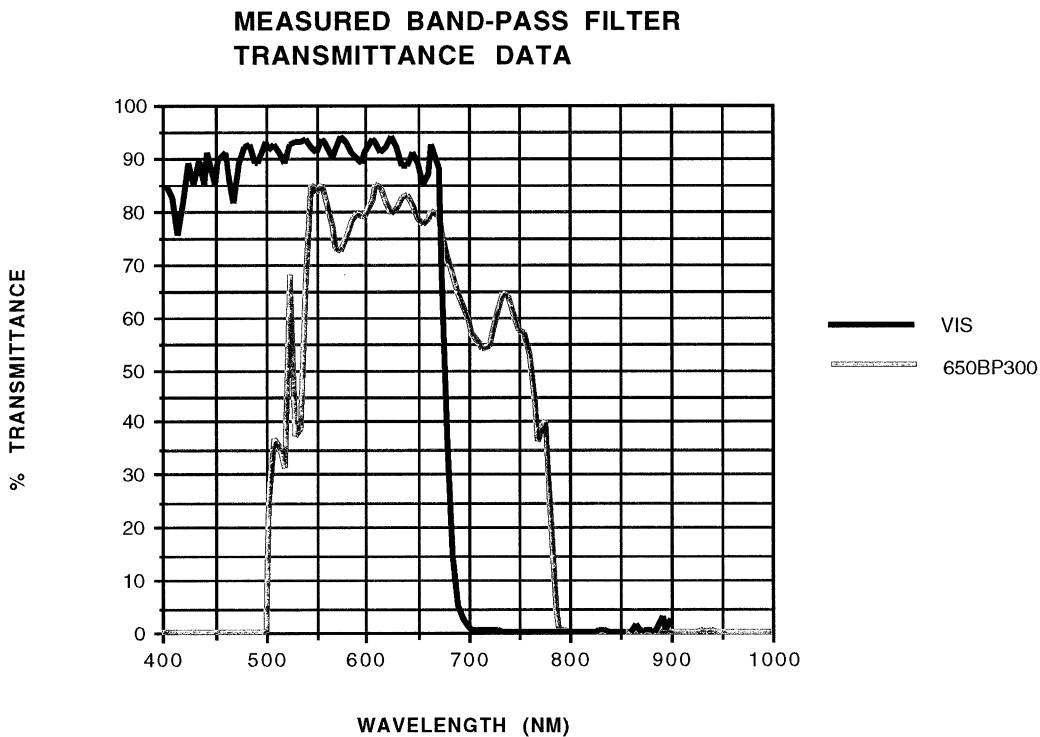


Figure 6: Band-pass Filter Transmittance Plot

The last major camera difference is found in the image-processing software. Both camera versions' software interpolates the raw color data to effectively give each pixel in the final image full, 24-bit color. In addition to the interpolation algorithms, the CIR driver backs-out the IR signal from the total signal captured by the red and green pixels, performs a color balance, and applies a false color registration. Therefore, the final infrared RGB image in file has the infrared signal in the red channel, the red signal in the green channel, and the green signal in the blue channel. This false color reassignment is the same assignment found in infrared film.

CIR Camera Specifications⁶

The following is a summary of the key CIR camera specifications:

Camera Body: Nikon N90

Pixel Size: $9 \mu\text{m} \times 9 \mu\text{m}$

Resolution(in pixel): 1012 x 1525 (420 model); 2056 x 3060 (460 model)

Spectral sensitivity: 400 nm - 1000 nm (no Filter)

400 nm - 700 nm (with VIS Filter)

500 nm - 800 nm (with IR Filter)

Dynamic Range: 36-bit color capture; 24-bit color stored

File Size: 4.5 MB (420 model); 18 MB (460 model)

3.2 Model Description

3.2.1 Atmospheric Section

Currently, the model has three different atmospheric options incorporated into it. All of the atmospheres have been generated using the USAF Modtran atmospheric model. Currently, the radiometric model's atmospheric options, are all Northeastern United States summer day models. The difference between the atmospheres is the amount of overcast and humidity in them. The three atmospheres are:

- 1) Clear summer day with 23 km visibility (Roch-23)
- 2) Summer day with 7 km visibility (Roch-7)
- 3) Summer day with only 5 km visibility and an additional 50% humidity added (Roch-5+).

The following five figures are plots of the Modtran out data from the three different atmospheres runs. Figure 7 is a plot of the three atmospheres exoatmospheric spectral irradiance. Figure 8 shows the downwelled solar radiance for the atmospheres. Figure 9 shows the upwelled solar radiance. Figures 10 and 11 are the atmospheric transmittance plots for the three atmospheres. Figure 10 displays the sun to target atmospheric transmittance and Figure 11 displays the target to sensor atmospheric transmittance.

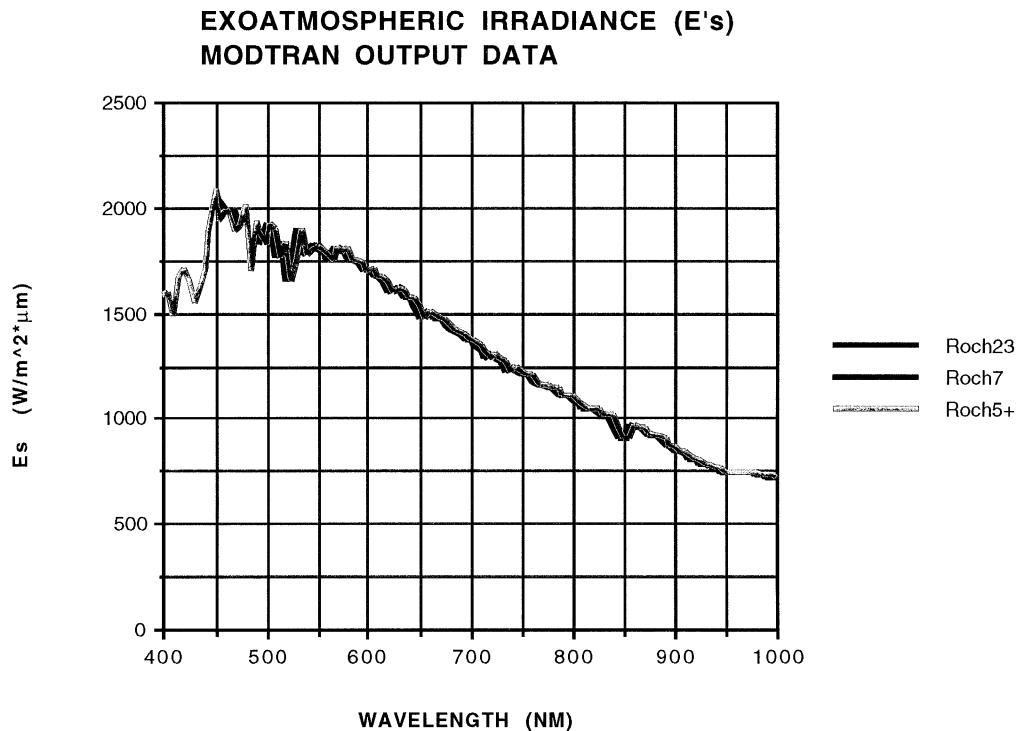


Figure 7: Exoatmospheric Spectral Irradiance Plot

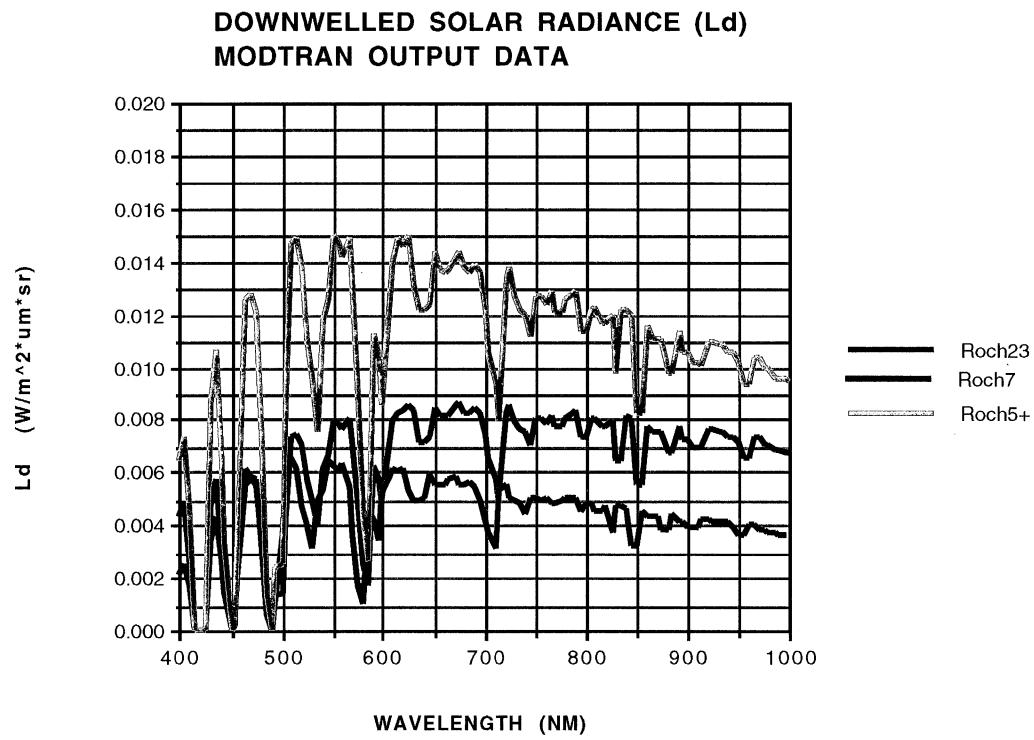


Figure 8: Downwelled Solar Radiance Plot

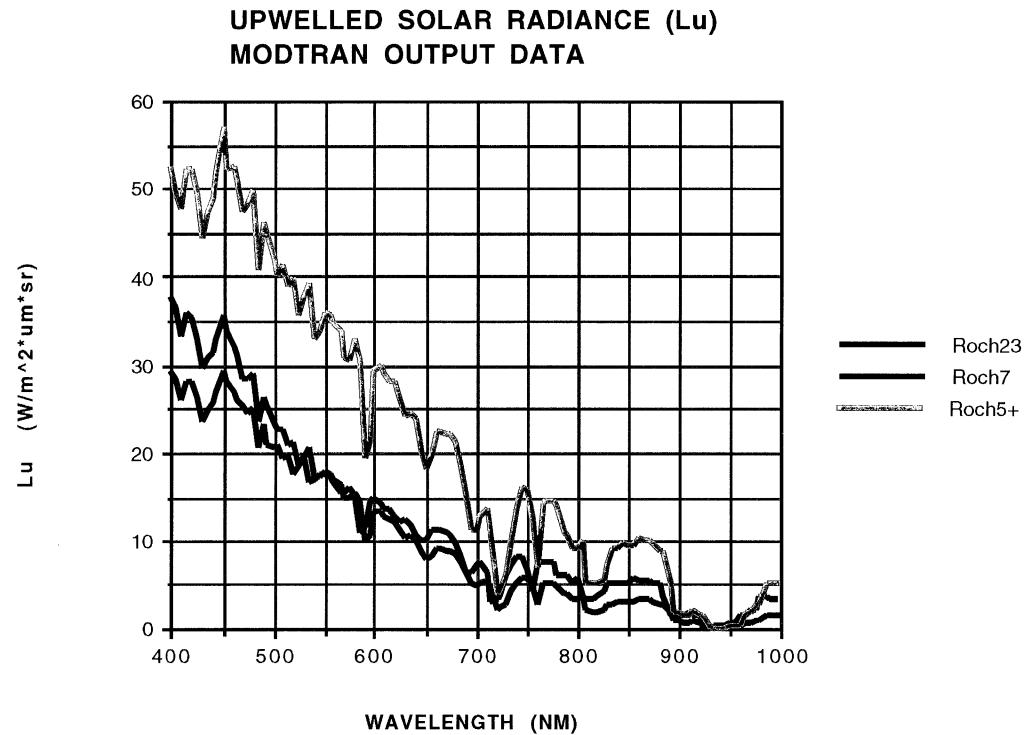


Figure 9: Upwelled Solar Radiance Plot

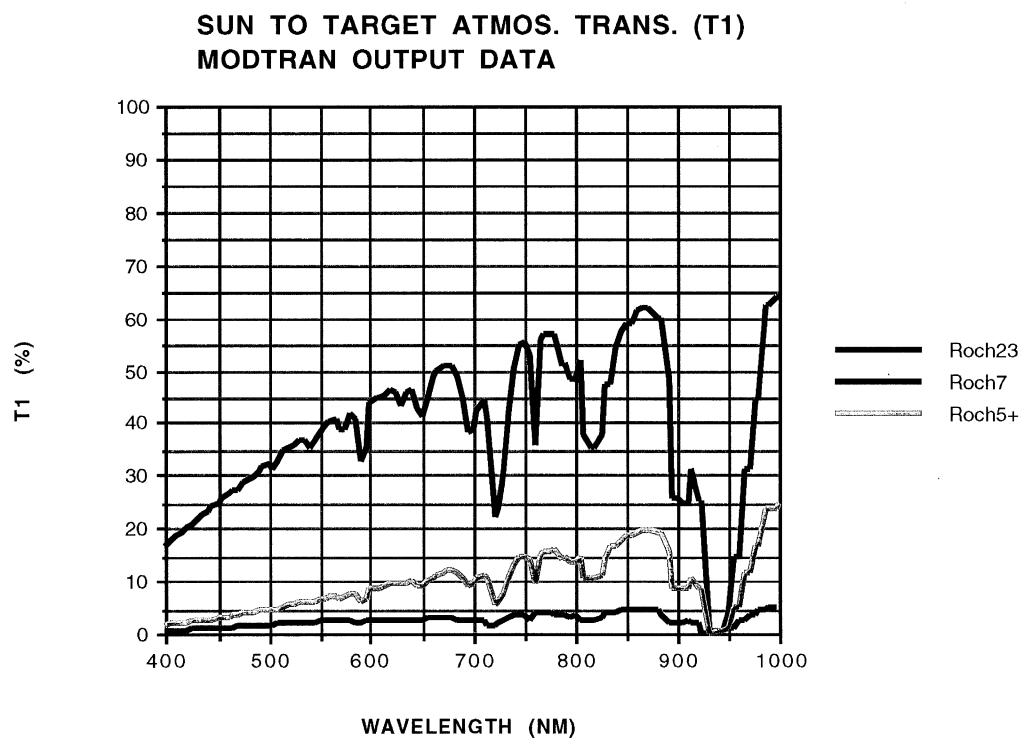


Figure 10: Sun to Target Atmospheric Transmittance Plot

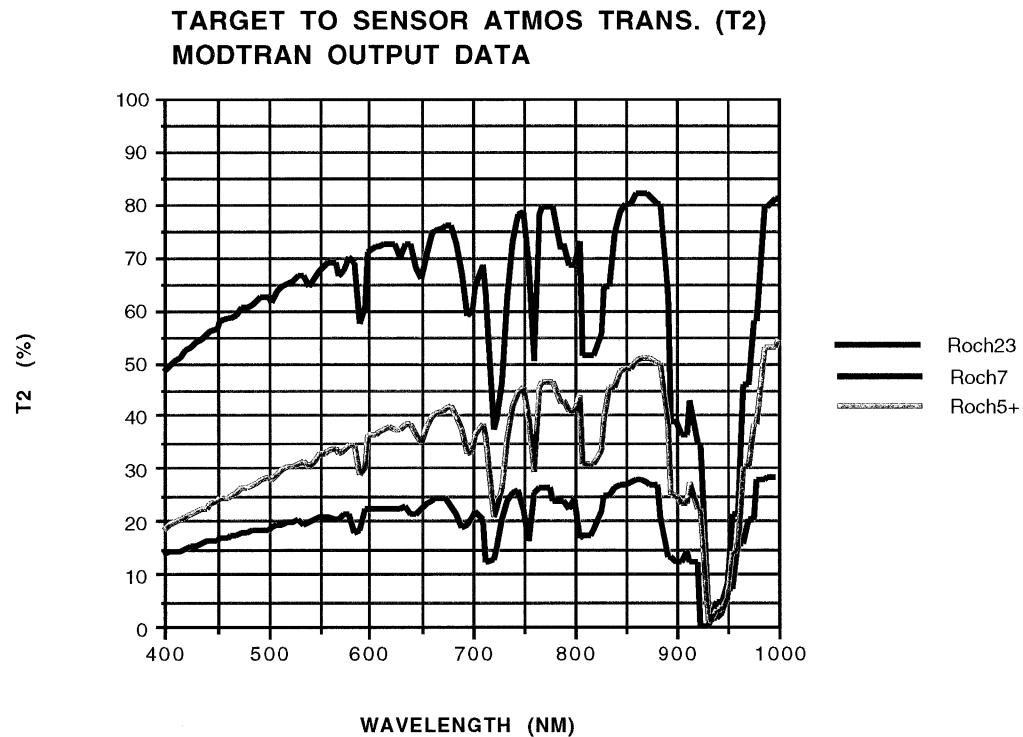


Figure 11: Target to Sensor Atmospheric Transmittance Plot

3.2.2 Ground Target Section

The model currently incorporates two main target source options, one man-made target and one natural target. The two targets are the Macbeth Colorchecker chart and Wheat reflectance data. The spectral reflectances of the targets were accurately measured between 400 nm and 1000 nm at 5 nm increments.

The Macbeth color checker is a well-known color standard used in the graphic arts and publishing industry. The Colorchecker consists of twenty-four different color patches. The patches consist of both a variety of colors and neutral gray levels. The Colorchecker typically comes in an oversize of 9 by 13 inches with individual patches of 1.75 by 1.75 inches. In 1996, Kodak contracted Macbeth to create a Colorchecker that has 1 meter by 1 meter size color patches and 2 meter by 2 meter gray patches. This mammoth version of the Colorchecker is for ground-truth analysis for aerial imaging. Figures 12 through 15 show the measured reflectances of the various patches.

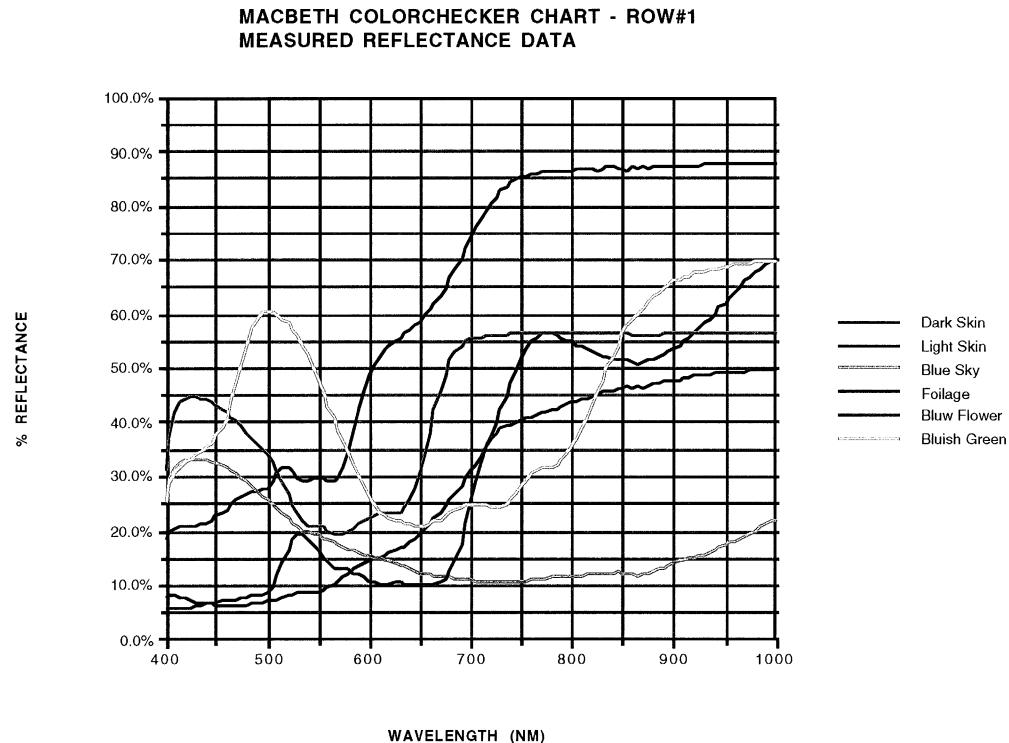


Figure 12: Macbeth Colorchecker Chart Row #1 Reflectance Plot

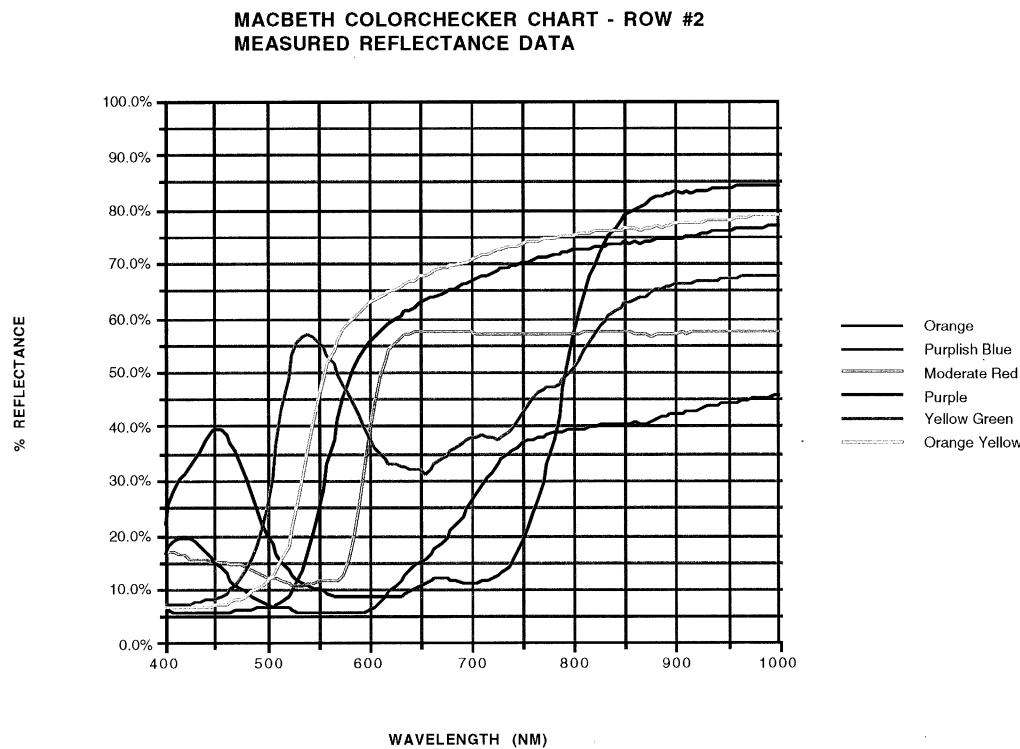


Figure 13: Macbeth Colorchecker Chart Row #2 Reflectance Plot

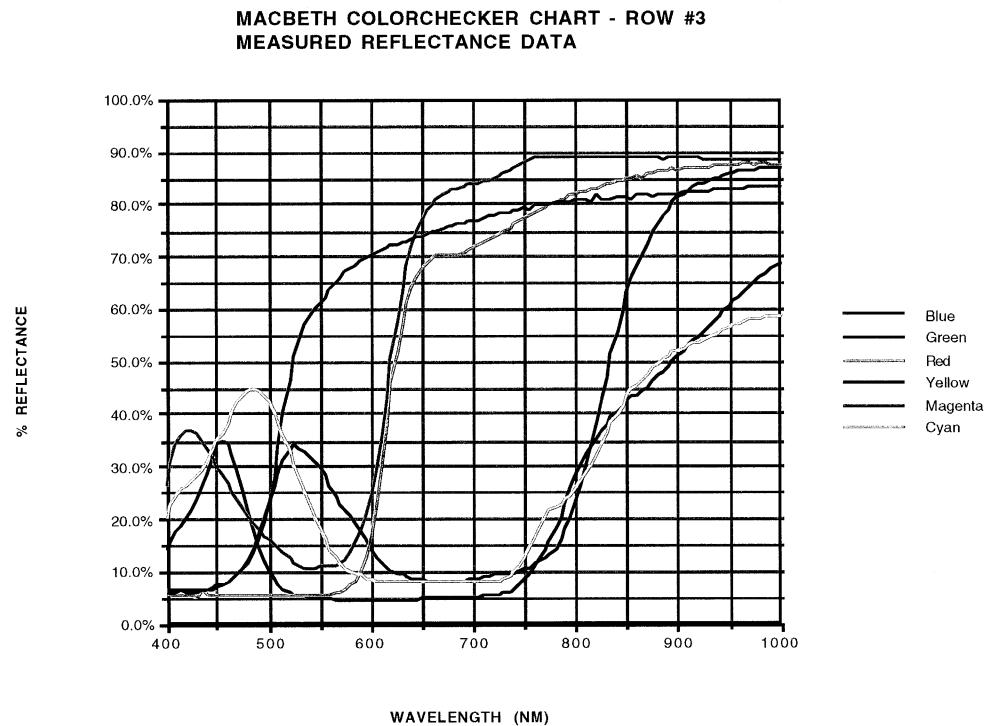


Figure 14: Macbeth Colorchecker Chart Row #3 Reflectance Plot

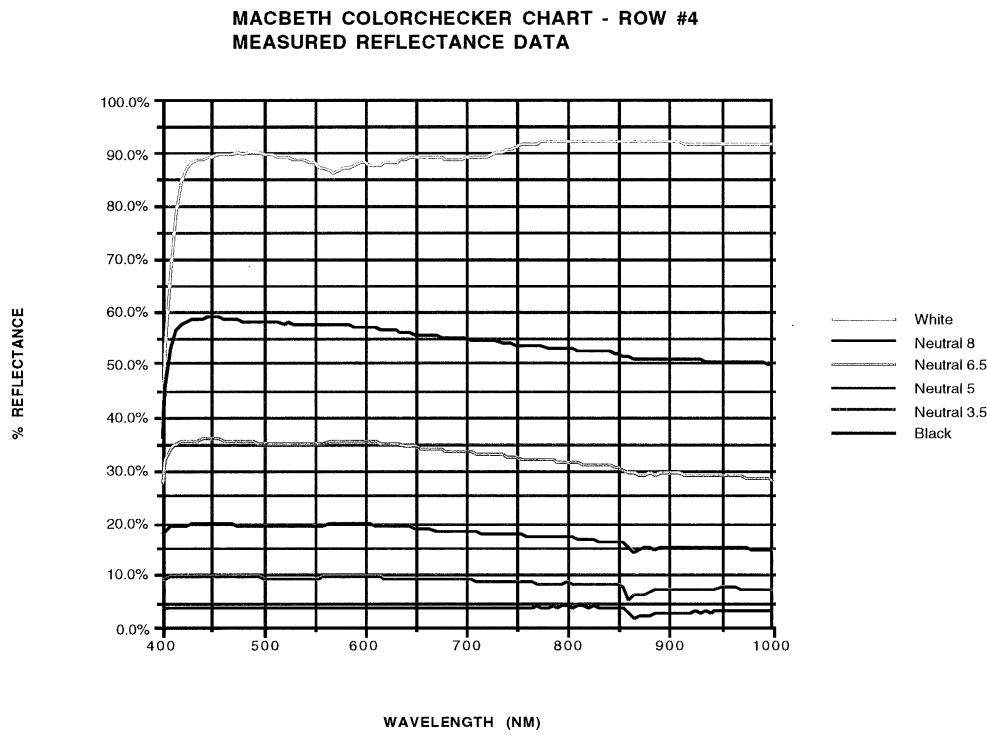


Figure 15: Macbeth Colorchecker Chart Row #4 Reflectance Plot

The second target spectra, measured wheat reflectance data, is composed of three stages of annual wheat growth. The reflectance curves of the three stages of growth are shown below in Figure 16.

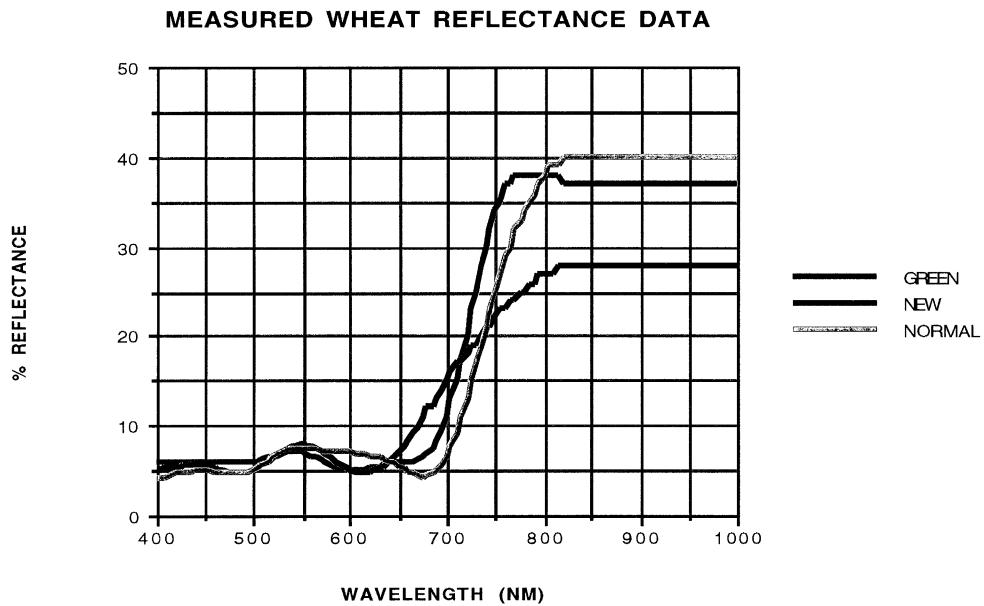


Figure 16: Wheat Reflectance Plot

3.2.3 Camera Section

The major technical characteristics of the CIR cameras have already been discussed. For completeness, a few remaining radiometric modeling considerations of the camera must still be addressed. The transmittance of the camera's lens must be incorporated into the radiometric model. The spectral transmittance of a 28 mm Nikon Nikkor lens was measured, and the data is shown in Figure 17 below. (Note, the anomaly around 875 nm is due to the spectrometer.)

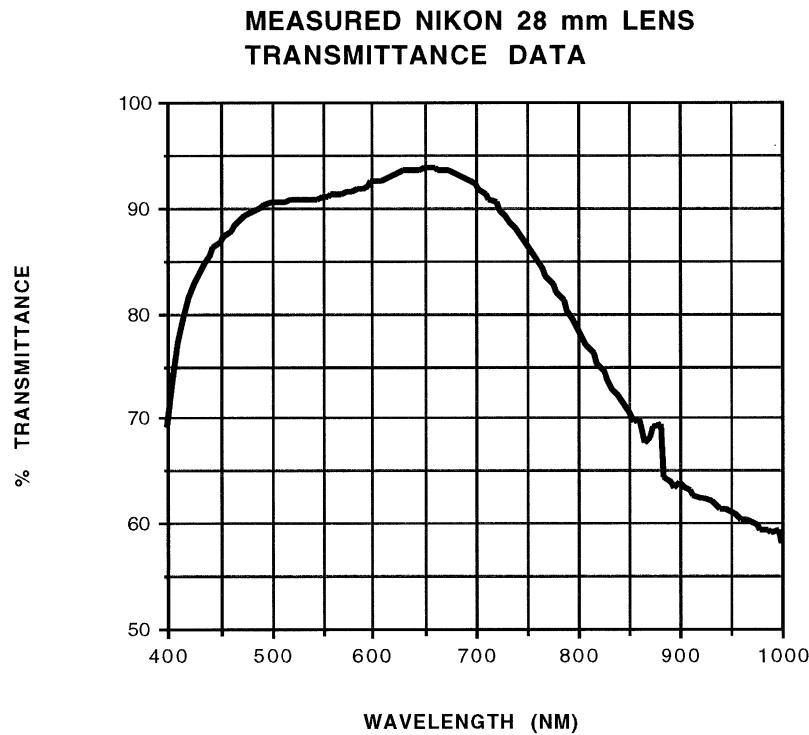


Figure 17: 28 mm Nikon Lens Transmittance Plot

The lens fall-off (fall-off of intensity as a function of field angle) was also measured and incorporated into the model by using a average COS^3 and COS^4 function (see Figure 18). This roll-off factor is important in comparing on-axis data to off-axis data. Since the 460 camera has a significantly larger field than the 420 version, the lens roll-off will have a much larger impact in final performance. As shown below in Figure 18, the 460 camera's energy falls off substantially out in the field. The model uses a LUT for lens roll-off prediction. Currently, the model assumes a lens focal length of 28 mm and is capable of predicting on-axis, half-field, and full-field point radiometric performance.

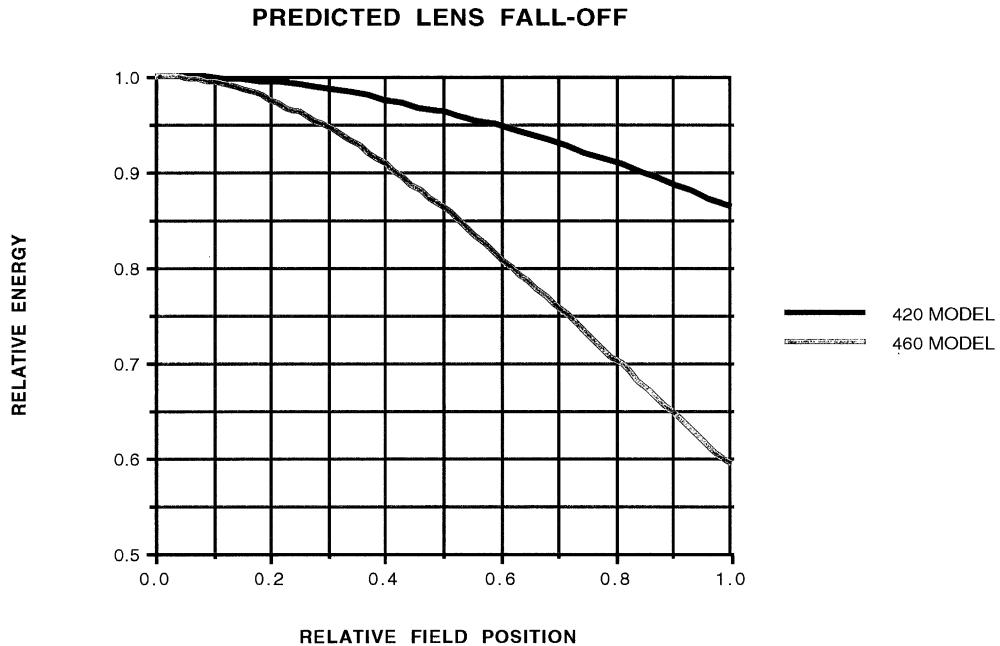


Figure 18: 28 mm Lens Fall-Off Plot

Figure 19 shows the Lens MTF of the Nikon 28 mm lens. The Nikon lens was measured with the 650BP300 band-pass filter screwed onto it. This data was taken at half-field in the radial direction. The focus position was kept at the on-axis best focus point. The top curve is the F/5.6 diffraction limited lens¹⁴. Notice that the Nikon lens is far from being diffraction limited. This lens is typical for off-the-shelf consumer lenses.

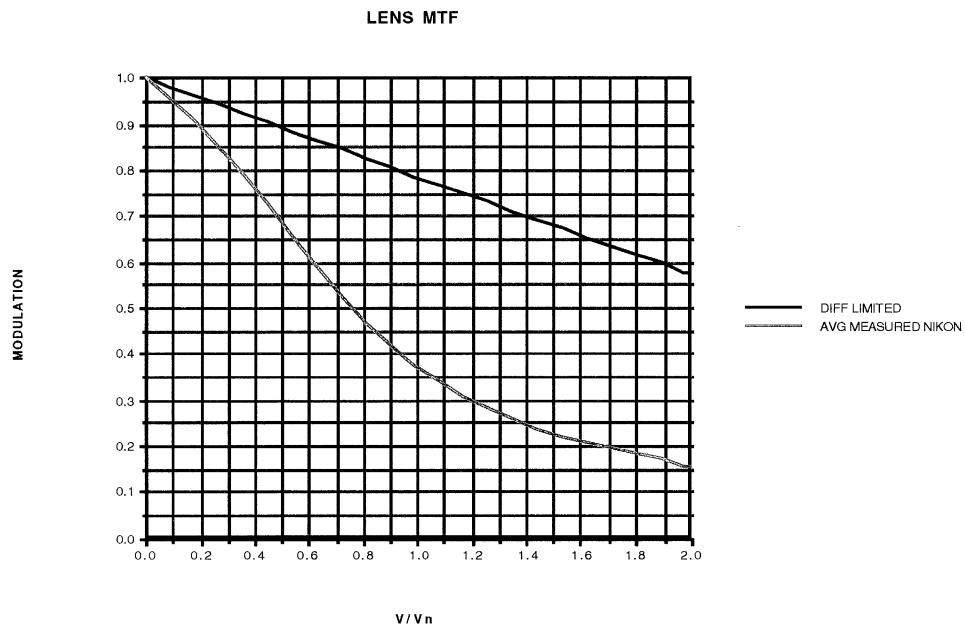


Figure 19: Lens MTF Plot

Figure 20 shows the driver interpolation MTF for the three color pixels. The interpolation MTF is a result of the Bayer pattern architecture¹. The interpolation MTF is scene dependent and is therefore modeled as a weighted average MTF. The red pixel and blue pixel MTFs are identical. Note, the red and blue pixels are intrinsically influenced by the green pixel. The resulting MTF curves are clearly color distinct. Because of this MTF color distinction, some images will suffer from color aliasing of some objects. The presence of color aliasing can be seen in Table 4 of the Results section of this paper .

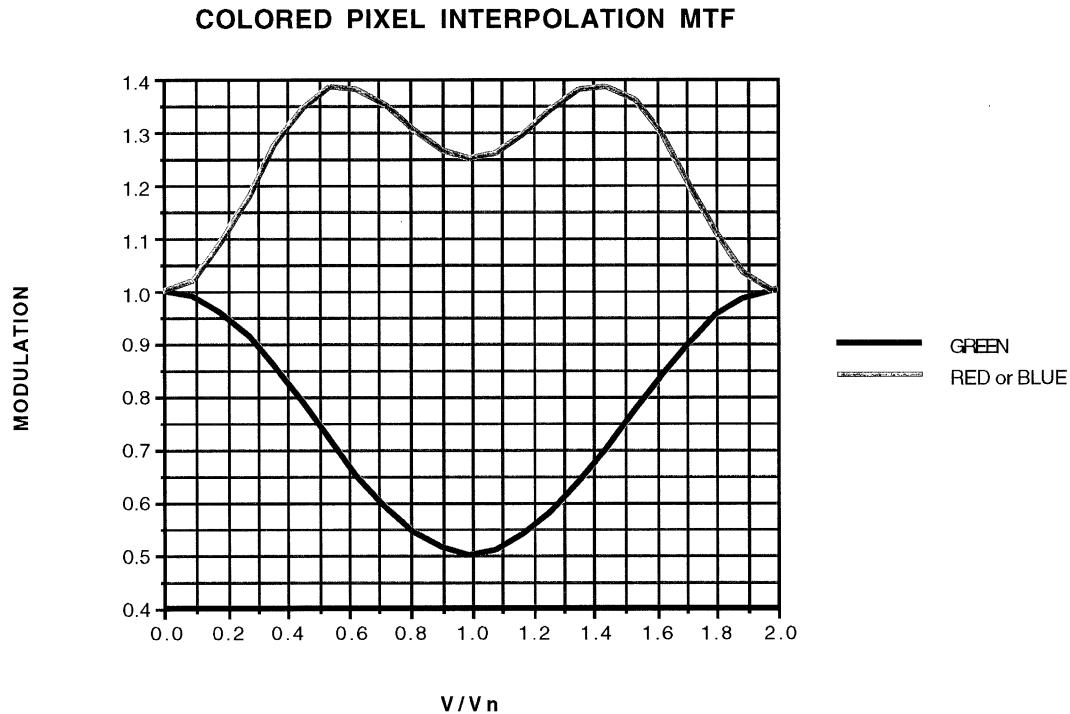


Figure 20: Color Interpolation MTF Plot

3.2.4 Radiometric Model Equations

The following two sub-sections (3.2.4 and 3.2.5) rigorously define and detail the equations used in the model. Sub-sections 3.2.4 concentrates on the equations used in the radiometric portion of the model. The main reference sources for these equations are: Schott¹³, Dereniak and Crowe⁴, Boyd², and Ekiert⁹. These equations analytically describe the radiometric attributes of the entire imaging chain (from the sun's radiation to the target's reflectance to the camera's digital count output).

Total spectral solar radiance reaching the front of the sensor¹³: $L_{\text{sensor-frt}}$ [watts / (meter² * micron * steradian)]

$$L_{\text{sensor-frt}}(\lambda) = E'_s(\lambda) * \tau_1(\lambda) * \cos(\sigma) * (r(\lambda)/\pi) * \tau_2(\lambda) + \tau_2(\lambda) * r(\lambda) * L_d(\lambda) + L_u(\lambda) \quad (\text{R1})$$

where:

$E'_s(\lambda)$ is the exoatmospheric irradiance [watts / (meter² * micron)]

$\tau_1(\lambda)$ is the atmospheric spectral transmittance along the sun to target path [%]

σ is the solar zenith angle [degrees]

$r(\lambda)$ is the target spectral reflectance [%]

$\tau_2(\lambda)$ is the atmospheric spectral transmittance along the target to sensor path [%]

$L_d(\lambda)$ is the downwelled solar radiance [watts / (meter² * micron * steradian)]

$L_u(\lambda)$ is the path solar radiance [watts / (meter² * micron * steradian)]

-or - the total spectral solar radiance reaching the front of the sensor can be expressed in terms of its signal and haze components:

$$L_{\text{sensor-frt}}(\lambda) = L_{\text{sensor-frt,signal}}(\lambda) + L_{\text{sensor-frt,haze}}(\lambda) \quad (\text{R2})$$

where:

$L_{\text{sensor-frt,signal}}(\lambda) = E'_s(\lambda) * \tau_1(\lambda) * \cos(\sigma) * (r(\lambda)/\pi) * \tau_2(\lambda) + \tau_2(\lambda) * r(\lambda) * L_d(\lambda)$

$L_{\text{sensor-frt,haze}}(\lambda) = L_u(\lambda)$

Total irradiance at the detector (or pixel)^{2,4,13}; $E_{\text{e,det}}(\lambda)$ [watts / (meter² * micron)]

$$E_{\text{e,det}}(\lambda) = \pi * L_{\text{sensor-frt}}(\lambda) * T_{\text{bpf}}(\lambda) * T_{\text{lens}}(\lambda) / ((4 * F/\#^2) + 1) \quad (\text{R3})$$

where:

$L_{\text{sensor-frt}}(\lambda)$ is the total spectral radiance reaching the front of the sensor

T_{bpf} is the spectral transmittance of the band-pass filter in front of the lens [%]

T_{lens} is the spectral transmittance of the lens [%]

$F/\#$ is F number of the lens = focal length / entrance pupil diameter

- or - the total irradiance at the detector (or pixel); can be expressed in terms of its signal and haze components:

$$E_{e,det}(\lambda) = E_{e,det,signal}(\lambda) + E_{e,det,haze}(\lambda) \quad (R4)$$

where:

$$\begin{aligned} E_{e,det,signal}(\lambda) &= \pi * L_{\text{sensor-frt,signal}}(\lambda) * T_{\text{bpf}}(\lambda) * T_{\text{lens}}(\lambda) / ((4 * F/\#^2) + 1) \\ E_{e,det,haze}(\lambda) &= \pi * L_{\text{sensor-frt,haze}}(\lambda) * T_{\text{bpf}}(\lambda) * T_{\text{lens}}(\lambda) / ((4 * F/\#^2) + 1) \end{aligned}$$

Total irradiance at the detector (or pixel)⁴; $E_{p,det}(\lambda)$
[photons / (meter² * micron * second)]

$$E_{p,det}(\lambda) = E_{e,det}(\lambda) * \lambda / (h * c) \quad (R5)$$

where:

$$\begin{aligned} \lambda &= \text{emitted photon wavelength [microns]} \\ h &= \text{Planck's constant } (6.6262 \times 10^{-34} \text{ Wsec}^2) \\ c &= \text{speed of light } (2.999 \times 10^8 \text{ m/sec}) \end{aligned}$$

-or-

$$E_{p,det}(\lambda) = E_{p,det,signal} + E_{p,det,haze} \quad (R6)$$

where:

$$\begin{aligned} E_{p,det,signal}(\lambda) &= E_{e,det,signal}(\lambda) * \lambda / (h * c) \\ E_{p,det,haze}(\lambda) &= E_{e,det,haze}(\lambda) * \lambda / (h * c) \end{aligned}$$

Total electrons due to solar radiation for a given wavelength; e_{num}
[electrons]

$$e_{\text{num}}(\lambda) = E_{p,det}(\lambda) * \eta(\lambda) * A_{\text{det}} \quad (R7)$$

where:

$$E_{p,det}(\lambda) \text{ [photons / (meter}^2 \text{ * micron * second)]}$$

$\eta(\lambda)$ is the quantum efficiency of the detector [%]

A_{det} is the area of the detector or pixel [meter²]

-or-

$$e_{\text{num}}(\lambda) = e_{\text{num,signal}}(\lambda) + e_{\text{num,haze}}(\lambda) \quad (\text{R8})$$

where:

$$\begin{aligned} e_{\text{num,signal}}(\lambda) &= E_{\text{p,det,signal}}(\lambda) * \eta(\lambda) * A_{\text{det}} \\ e_{\text{num,haze}}(\lambda) &= E_{\text{p,det,haze}}(\lambda) * \eta(\lambda) * A_{\text{det}} \end{aligned}$$

Total electrons due to solar radiation for a given wavelength band; $e_{\text{num,wb}}$ [electrons]

$$e_{\text{num,wb}}(\lambda) = e_{\text{num}}(\lambda) * \Delta_\lambda \quad (\text{R9})$$

where:

$e_{\text{num}}(\lambda)$ is the number of electrons for a given wavelength
 Δ_λ is the wavelength bandwidth [microns]

-or-

$$e_{\text{num,wb}}(\lambda) = e_{\text{num,wb,signal}}(\lambda) + e_{\text{num,wb,haze}}(\lambda) \quad (\text{R10})$$

where:

$$\begin{aligned} e_{\text{num,wb,signal}}(\lambda) &= e_{\text{num,signal}}(\lambda) * \Delta_\lambda \\ e_{\text{num,wb,haze}}(\lambda) &= e_{\text{num,haze}}(\lambda) * \Delta_\lambda \end{aligned}$$

Total number of electrons at the detector or pixel due to solar radiation; e_{det} [electrons]

$$e_{\text{det}} = \sum e_{\text{num,wb}}(\lambda) ; \text{ summed over the defined wavelength band} \quad (\text{R11})$$

-or-

$$e_{\text{det}} = \sum (e_{\text{num,wb,signal}}(\lambda) + e_{\text{num,wb,haze}}(\lambda)) \quad (\text{R12})$$

Total number of electrons for a monochrome pixel; $e_{\text{det,m}}$ [electrons]

$$e_{\text{det,m}} = e_{\text{det}} \quad \text{-or-} \quad (\text{R13})$$

$$e_{\text{det,m}} = e_{\text{det,m,signal}} + e_{\text{det,m,haze}} \quad (\text{R14})$$

Total number of electrons for a red pixel due to solar radiation; $e_{det,r}$ [electrons]

$$e_{det,r} = \sum (T_{cfa,r}(\lambda) * e_{num,wb}(\lambda)) ; \text{ summed over the defined wavelength band} \quad (R15)$$

where:

$T_{cfa,r}(\lambda)$ is the color filter array red pixel spectral transmittance [%]

-or-

$$e_{det,r} = e_{det,r,signal} + e_{det,r,haze} \quad (R16)$$

where:

$$\begin{aligned} e_{det,r,signal} &= \sum (T_{cfa,r}(\lambda) * e_{num,wb,signal}(\lambda)) \\ e_{det,r,haze} &= \sum (T_{cfa,r}(\lambda) * e_{num,wb,haze}(\lambda)) \end{aligned}$$

likewise, the total number of electrons for the green and blue pixels due to solar radiation is computed in a similar manner.

Total RMS number of electrons due to sensor and electronic noise^{9,13}; $e_{s&enoise}$ [electrons]

$$e_{s&enoise} = \sqrt{(e_{sensornoise})^2 + (e_{shotnoise})^2 + (e_{quannoise})^2} \quad (R17)$$

where:

$e_{sensornoise}$ = sensor noise

$e_{shotnoise}$ = shot noise = $\sqrt{e_{det}}$

$e_{quannoise}$ = quantization noise = $e_{det} / (2^{\#bit} * \sqrt{12})$

where:

#bit = the number of bits (8 or 12)

Grand total number of electrons; e_{sum} [electrons]

$$e_{sum} = e_{det} + e_{s&enoise} \quad (R18)$$

Camera Digital Counts:

$$8\text{-bit counts for SIGNAL e's} = \text{ROUND}(e_{\text{det, signal}} / \Gamma) \quad (\text{R19})$$

$$8\text{-bit counts for HAZE e's} = \text{ROUND}(e_{\text{det,b,haze}} / \Gamma) \quad (\text{R20})$$

$$8\text{-bit counts for total (sig + haze) e's} = \text{ROUND}(e_{\text{det,b}} / \Gamma) \quad (\text{R21})$$

$$\begin{aligned} 8\text{-bit counts for total sensor and electronics noise e's} \\ = \text{ROUND}(e_{\text{s&enoise}} / \Gamma) \end{aligned} \quad (\text{R22})$$

$$8\text{bit counts for grand total e's} = \text{ROUND}(e_{\text{sum}} / \Gamma) \quad (\text{R23})$$

where:

$$\Gamma = \text{quantization interval} = (\partial / 2^{\#\text{bit}})$$

where: ∂ = detector saturation level in electrons

The 12-bit digital count equations are identical to the 8-bit equations, except the #bits = 12 instead of 8.

3.2.5 Image Quality Model Equations

Sub-section 3.2.5 outlines the equations for the image quality portion of the model. The main reference sources for these equations are: Ekiert⁹, Schott¹³, and Tantalo¹⁵. These equations analytically define all of the imaging chain component's contributions to the final image quality of the output image. By using a linear system approach (i.e. TMA), the model cascades all of the appropriate contributions to predict a final camera resolution.

Ground sample distance: GSD_{it}^{9,13}; GSD_{ct}

$$GSD_{it} = (P_{it} * A) / FL \quad (IQ1A)$$

$$GSD_{ct} = (P_{ct} * A) / FL \quad (IQ1B)$$

where;

P_{it} = in-track pixel size

P_{ct} = cross-track pixel size

A = aircraft altitude above the ground

FL = focal length of the lens

Nyquist limited ground resolving distance^{9,13}: GRD_{nyqt}

$$GRD_{nyqt,it} = 2 * GSD_{it} \quad (IQ2A)$$

$$GRD_{nyqt,ct} = 2 * GSD_{ct} \quad (IQ2B)$$

MTFs

v denotes the frequency for the in-track spatial direction

η denotes the frequency for the cross-track spatial direction

Atmospheric MTF: MTF_{atmos}(v); MTF_{atmos}(η)

$$MTF_{atmos}(v) = MTF_{atmos}(\eta) = \text{constant for all frequencies} \quad (IQ3)$$

Aircraft linear motion MTF: MTF_{aircraft}(v)^{9,13}; MTF_{aircraft}(η)

$$MTF_{aircraft}(v) = \text{sinc}(v * \nabla_{eqamt} * P_{it}) \quad (IQ4A)$$

where:

∇_{eqamt} = equivalent pixel factor = Ω / P_{it}

Ω_{it} = in-track smear amount = aircraft speed_{it} * integration time *(fl / ALT)

P_{it} = pixel size in the in-track direction

$$MTF_{aircraft}(\eta) = \text{sinc}(\eta * \nabla_{eqamt} * P_{ct}) \quad (IQ4B)$$

where:

∇_{eqamt} = equivalent pixel factor = Ω / P_{ct}

$$\Omega_{ct} = \text{cross-track smear amount} = \text{aircraft speed}_{ct} * \text{integration time} * (\text{fl / ALT})$$

$$P_{ct} = \text{Pixel size in the cross-track direction}$$

The following three figures, show the effects of integration time, aircraft speed, and altitude on the MTF_{aircraft}.

AIRCRAFT MOTION MTF (LINEAR SMEAR)
FL= 28 MM; PIXEL = 9 MIC; ALT. = 3000 FT; SPEED = 100 MPH

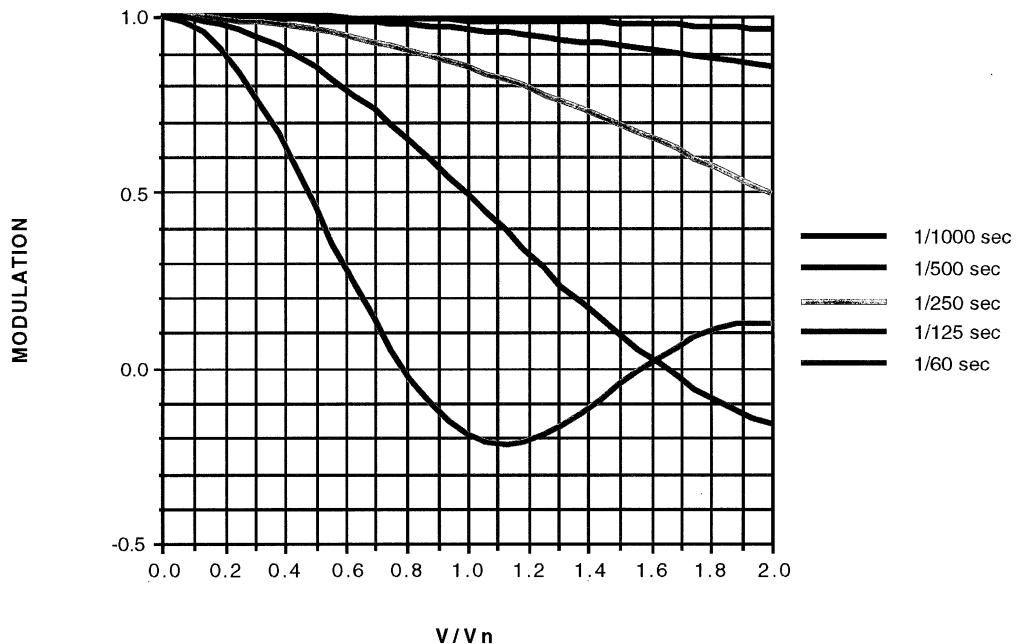


Figure 21: Aircraft Motion MTF for Various Integration Times Plot

AIRCRAFT MOTION MTF (LINEAR SMEAR)
FL = 28 MM; PIXEL = 9 MIC; ALT = 3000 FT; SHUTTER = 1/250 SEC

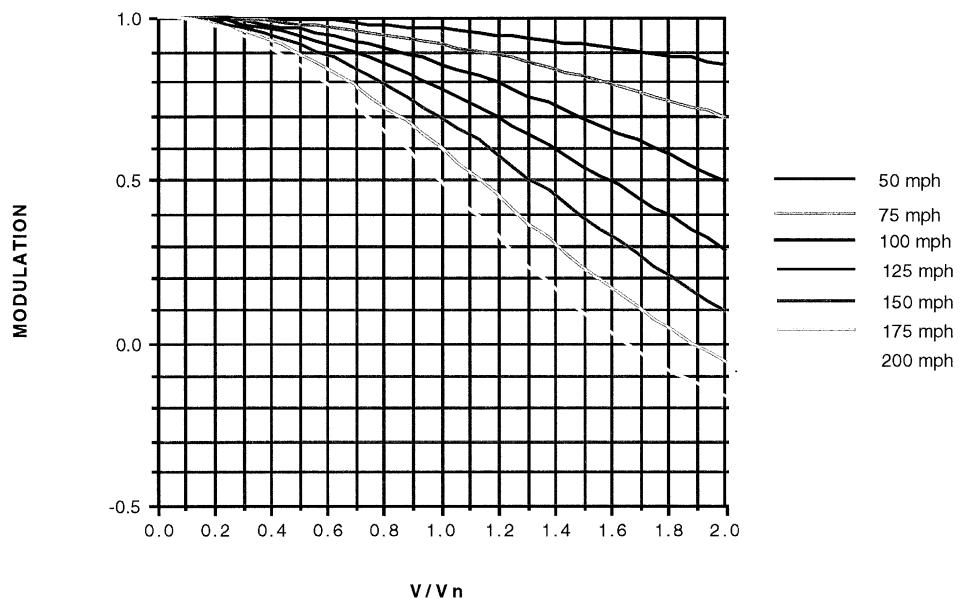


Figure 22: Aircraft Motion MTF for Various Aircraft Speeds Plot

AIRCRAFT MOTION MTF (LINEAR SMEAR)
FL = 28 MM; PIXEL = 9 MIC; SPEED = 100 MPH ; SHUTTER = 1/250 SEC

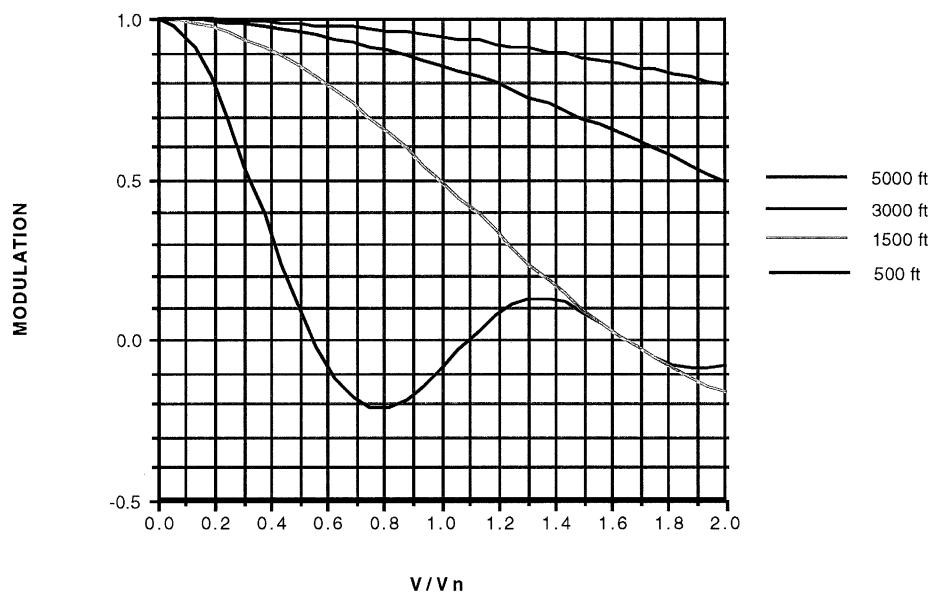


Figure 23: Aircraft Motion MTF for Various Aircraft Altitudes Plot

Optics MTF: Diffraction limited circular aperture lens MTF¹⁴: $\text{MTF}(v)_{\text{diffLens}}$

$$\text{MTF}(v)_{\text{diffLens}} = (2/\pi) * (\phi - \cos(\phi) * \sin(\phi)) * \cos(\theta)^k = \text{MTF}(\eta)_{\text{diffLens}} \quad (\text{IQ5})$$

where:

$$\phi = \cos^{-1}(v/v_o)$$

$$v_o = 1/(\lambda * F/\#)$$

θ = is the half angle

$k = 1$ for radial lines and 3 for tangential lines

Detector MTF: $\text{MTF}_{\text{det}}(v)^{9,13,15}$; $\text{MTF}_{\text{det}}(\eta)$

$$\text{MTF}_{\text{det}}(v) = \text{sinc}(v * P_{it}) \quad (\text{IQ6A})$$

where P_{it} = pixel size in the in-track direction

$$\text{MTF}_{\text{det}}(\eta) = \text{sinc}(\eta * P_{ct}) \quad (\text{IQ6B})$$

where: P_{ct} = pixel size in the cross-track direction

Charge transfer MTF: $\text{MTF}_{\text{chg}}(v)^9$; $\text{MTF}_{\text{chg}}(\eta)$

$$\text{MTF}_{\text{chg}}(v) = \text{EXP}[-\gamma_{it} (1-\epsilon)(1-\cos(\alpha_{it}))] \quad (\text{IQ7A})$$

where: γ_{it} = # of charge transfers in the in-track direction

ϵ = charge transfer efficiency

$$\alpha_{it} = 2 * \pi * P_{it} * v$$

$$\text{MTF}_{\text{chg}}(\eta) = \text{EXP}[-\gamma_{ct} (1-\epsilon)(1-\cos(\alpha_{ct}))] \quad (\text{IQ7B})$$

where: γ_{ct} = # of charge transfers in the in-track direction

ϵ = charge transfer efficiency

$$\alpha_{ct} = 2 * \pi * P_{ct} * \eta$$

Detector clocking MTF: $\text{MTF}_{\text{clock}}(v)^9$; $\text{MTF}_{\text{clock}}(\eta)$

$$\text{MTF}_{\text{clock}}(v) = \text{sinc}(v * P_{it}/\Phi_{\text{clock}}) \quad (\text{IQ8A})$$

$$\text{MTF}_{\text{clock}}(\eta) = \text{sinc}(\eta * P_{ct}/\Phi_{\text{clock}}) \quad (\text{IQ8B})$$

where: Φ_{clock} = # of phase clocks

Interpolation MTF (weighted average MTF)¹:

Green interpolation: $\text{MTF}_{\text{interp,grn}}(v)$; $\text{MTF}_{\text{interp,grn}}(\eta)$

$$\text{MTF}_{\text{interp,grn}}(v) = 0.75 + (0.25 * \cos(2 * \pi * v/(2 * v_n))) \quad (\text{IQ9A})$$

$$\text{MTF}_{\text{interp,grn}}(\eta) = 0.75 + (0.25 * \cos(2 * \pi * \eta/(2 * \eta_n))) \quad (\text{IQ9B})$$

where:

$$v_n = \text{Nyquist frequency} = 1/(2 * P_{it})$$

$$\eta_n = \text{Nyquist frequency} = 1/(2 * P_{ct})$$

Red interpolation: $\text{MTF}_{\text{interp,red}}(v)$; $\text{MTF}_{\text{interp,red}}(\eta)$

$$\begin{aligned} \text{MTF}_{\text{interp,red}}(v) &= \text{MTF}_{\text{interp,grn}}(v) + (0.5 + (2 * (-0.1875)) * \cos(2 * \pi * v/(2 * v_n))) + \\ &\quad (2 * (-0.0625)) * \cos(4 * \pi * v/(2 * v_n)) \end{aligned} \quad (\text{IQ10A})$$

$$\begin{aligned} \text{MTF}_{\text{interp,red}}(\eta) &= \text{MTF}_{\text{interp,grn}}(\eta) + (0.5 + (2 * (-0.1875)) * \cos(2 * \pi * \eta/(2 * \eta_n))) + \\ &\quad (2 * (-0.0625)) * \cos(4 * \pi * \eta/(2 * \eta_n)) \end{aligned} \quad (\text{IQ10B})$$

Blue interpolation: $\text{MTF}_{\text{interp,blue}}(v)$; $\text{MTF}_{\text{interp,blue}}(\eta)$

$$\text{MTF}_{\text{interp,blue}}(v) = \text{MTF}_{\text{interp,red}}(v) \quad (\text{IQ11A})$$

$$\text{MTF}_{\text{interp,blue}}(\eta) = \text{MTF}_{\text{interp,red}}(\eta) \quad (\text{IQ11B})$$

Threshold Modulation Analysis⁹

Input modulation: ITM

$$\text{ITM} = \text{MTF}_{\text{atmos}} * \text{MTF}_{\text{aircraft}} * \text{MTF}_{\text{optics}} * \text{MOD}_{\text{target}} \quad (\text{IQ12})$$

where:

$$\text{MOD}_{\text{target}} = \text{target modulation} = (C - 1) / (C + 1) \quad (\text{IQ13})$$

$$C = \text{target to background contrast} = \text{NDVI}_{\text{target}} / \text{NDVI}_{\text{background}} \quad (\text{IQ14})$$

Required modulation: TM

$$\text{TM} = (\sqrt{(\text{SNR}_{\text{req}} * \text{MOD}_{\text{noise}})^2 + \text{TM}_{\text{vis}}}) / (\text{MTF}_{\text{det}} * \text{MTF}_{\text{chg}} * \text{MTF}_{\text{clock}} * \text{MTF}_{\text{elec}} * \text{MTF}_{\text{interp}}) \quad (\text{IQ15})$$

where:

$$\text{SNR}_{\text{req}} = \text{required minimum SNR for the eye}$$

$$\text{MOD}_{\text{noise}} = \text{noise modulation} = e_{\text{s&enoise}} / e_{\text{det,sig}} \quad (\text{IQ16})$$

where:

$$e_{\text{s&enoise}} = \text{total RMS number of electrons due to sensor \& electronic noise}$$

$$e_{\text{det,sig}} = \text{total number of electrons due to signal}$$

$$\text{TM}_{\text{vis}} = \text{required minimum modulation for the eye}$$

4.0 Results

4.1 Flight Test Data

Figure 21 shows the results of flight test raw image going through two different Photoshop drivers. The flight test image (see Appendix 1) is the large Macbeth target @ ≈ 1300 feet AGL with the 28 mm lens. The X-axis is the average reflectance of the neutral gray patches. The CIR v3.0.1 with gamma = 1.0 driver and a linear driver. The CIR driver is a standard CIR driver that comes with the camera. The linear driver is a driver that can be obtained by special request. Note the linear driver does not backout the infrared signal from the red and green pixels channels.

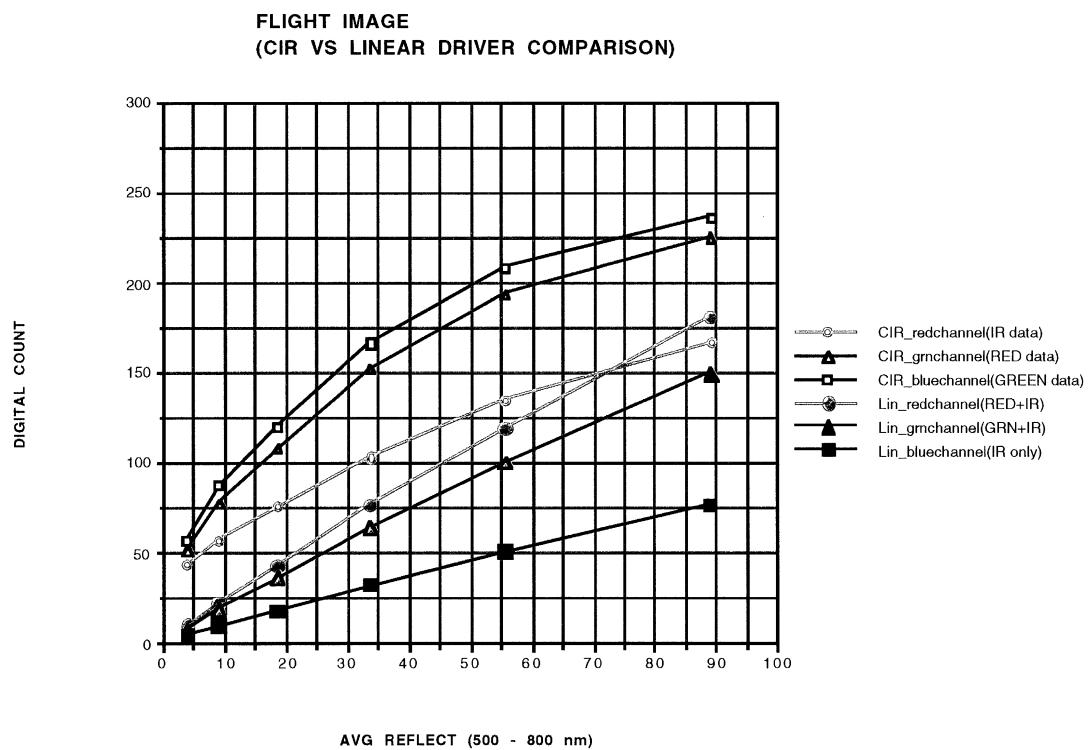


Figure 24: Driver Comparison Plot

4.2 Modeling Case Study - Three Wheat Curves

A modeling case study of wheat changes throughout the growing season was performed. The case study was used to show the utility of a CIR camera and the analytical model. The study compared the three temporal wheat curves shown previously in Figure 16. The study had the following input parameters:

Camera:	460 CIR
Filter:	650BP300
Lens:	28 mm
F#:	F/5.6
Integration Time:	0.002, 0.004, 0.0067, 0.008, 0.01667 sec.
Altitude:	3000 feet
Aircraft Speed:	50, 100, 150, 200, 250, 300, 350 mph
Target:	Wheat data (Figure 16)
Atmosphere:	Roch-23, Roch-7, Roch-5+
Field of View:	On-axis; Half-Field, Full-Field
Solar Angle:	30 degree

The results of the study are shown in the following four tables. The first three tables are radiometric summaries while the fourth table is an image quality summary for the study. Table 1 summarizes the camera response differences from the different wheat inputs.

***** WHEAT DIFFERENTIATION *****											
CAMERA -> 460		MATRIX RED MATRIX GRN MATRIX BLUE NDVI									
ATMOS -> ROCH-23		REL.	FLD	MATRIX (RED)		MATRIX (GREEN)		MATRIX (IR)		NDVI	
FILTER ->	650BP			expos.	tot'l	sig'l	tot'l	sig'l	tot'l	sig'l	tot'l
F/# ->	F/5.6										
TARGET ->	WHEAT-GRN	0.0	0.002	22	8	23	4	74	64	0.542	0.778
SUN ZEN ->	30	0.0	0.004	44	16	46	8	148	128	0.542	0.778
		0.0	0.0067	73	27	77	13	246	213	0.542	0.775
		0.0	0.008	88	32	92	16	296	256	0.542	0.778
		0.0	0.01667	183	66	191	34	615	533	0.541	0.780
CAMERA -> 460		MATRIX RED MATRIX GRN MATRIX BLUE NDVI									
ATMOS ->	ROCH-23	REL.	FLD	MATRIX (RED)		MATRIX (GREEN)		MATRIX (IR)		NDVI	
FILTER ->	650BP			expos.	tot'l	sig'l	tot'l	sig'l	tot'l	sig'l	tot'l
F/# ->	F/5.6										
TARGET ->	WHEAT-NEW	0.0	0.0067	108	62	89	25	180	147	0.250	0.407
SUN ZEN ->	30	0.0	0.008	130	74	106	31	216	177	0.249	0.410
		0.0	0.01667	271	154	221	64	450	369	0.248	0.411
CAMERA -> 460		MATRIX RED MATRIX GRE MATRIX BLUE NDVI									
ATMOS ->	ROCH-23	REL.	FLD	MATRIX (RED)		MATRIX (GREEN)		MATRIX (IR)		NDVI	
FILTER ->	650BP			expos.	tot'l	sig'l	tot'l	sig'l	tot'l	sig'l	tot'l
F/# ->	F/5.6										
TARGET ->	WHEAT-NORM	0.0	0.0067	66	20	88	24	201	168	0.506	0.787
SUN ZEN ->	30	0.0	0.008	79	24	105	29	241	202	0.506	0.788
		0.0	0.01667	165	49	219	61	503	421	0.506	0.791

Table 1: Wheat Differentiation

Table 2 below shows that the impact on NDVI due to lens fall-off is insignificant. While the lens fall-off does not impact the NDVI prediction, it will have a large impact on mosaicing images together. If the fall-off is not corrected for, the resultant mosaic will have dark sections butted to light sections.

***** LENS FALL-OFF EFFECT *****														
		REL.	FLD	expos.	MATRIX RED		MATRIX GRN		MATRIX BLUE		NDVI			
					(RED)	(GREEN)	(IR)							
CAMERA -> 460														
ATMOS ->	ROCH-23													
FILTER ->	650BP	TARGET ->	WHEAT-GRN	SUN ZEN ->	0.0	0.0067	73	27	77	13	246	213	0.542	0.775
F/# ->	F/5.6				0.5	0.00667	63	23	66	12	213	184	0.543	0.778
					1.0	0.00667	44	16	46	8	146	127	0.537	0.776
CAMERA -> 460														
ATMOS ->	ROCH-23													
FILTER ->	650BP	TARGET ->	WHEAT-NEW	SUN ZEN ->	0.0	0.0067	108	62	89	25	180	147	0.250	0.407
F/# ->	F/5.6				0.5	0.00667	94	53	77	22	156	127	0.248	0.411
					1.0	0.00667	65	37	53	15	107	88	0.244	0.408
CAMERA -> 460														
ATMOS ->	ROCH-23													
FILTER ->	650BP	TARGET ->	WHEAT-NORM	SUN ZEN ->	0.0	0.0067	66	20	88	24	201	168	0.506	0.787
F/# ->	F/5.6				0.5	0.00667	57	17	76	21	174	145	0.506	0.790
					1.0	0.00667	39	12	52	14	120	100	0.509	0.786

Table 2: Lens Fall-off Affect on NDVI Predictions

Table 3 shows the effects of different atmospheres on the imaging process. Atmospheres Roch-7 and Roch-5+ give some spurious results. This indicates that the two atmospheres are too water saturated for good imaging results.

***** ATMOSPHERIC EFFECT *****											
CAMERA -> 460		MATRIX RED MATRIX GRN MATRIX BLUE NDVI									
				(RED)		(GREEN)		(IR)			
F/# ->	F/5.6	ATMOS	expos.	tot'l	sig'l	tot'l	sig'l	tot'l	sig'l	tot'l	sig'l
TARGET ->	WHEAT-GRN	roch-23	0.01667	183	66	191	34	615	533	0.541	0.780
SUN ZEN ->	30	roch-7	0.01667	136	1	160	0	109	10	-0.110	0.810
		roch-5+	0.01667	265	2	320	0	252	66	-0.025	0.941
CAMERA -> 460		MATRIX RED MATRIX GRN MATRIX BLUE NDVI									
		(RED)		(GREEN)		(IR)					
F/# ->	F/5.6	ATMOS	expos.	tot'l	sig'l	tot'l	sig'l	tot'l	sig'l	tot'l	sig'l
TARGET ->	WHEAT-NEW	roch-23	0.01667	271	154	221	64	450	369	0.248	0.411
SUN ZEN ->	30	roch-7	0.01667	137	2	160	1	106	6	-0.128	0.5
		roch-5+	0.01667	276	13	323	3	231	44	-0.089	0.544
CAMERA -> 460		MATRIX RED MATRIX GRN MATRIX BLUE NDVI									
		(RED)		(GREEN)		(IR)					
F/# ->	F/5.6	ATMOS	expos.	tot'l	sig'l	tot'l	sig'l	tot'l	sig'l	tot'l	sig'l
TARGET ->	WHEAT-NORM	roch-23	0.01667	165	49	219	61	503	421	0.506	0.791
SUN ZEN ->	30	roch-7	0.01667	135	1	160	1	107	8	-0.116	0.778
		roch-5+	0.01667	264	1	323	2	239	52	-0.05	0.962

Table 3: Atmospheric Impact on NDVI Predictions

Table 4 shows results of the image quality analysis. Note, the NDVI calculated in the radiometric analysis was used to compute the target contrast. The table clearly shows the WHEAT-GRN can easily be distinguished from the WHEAT-NEW. The WHEAT-GRN and the WHEAT-NORM are too similar to easily detect the difference. Note that for various aircraft speed, various components of the imaging change dominate the results. Also, note the presence of color aliasing as seen from the differences in GRD between the green and blue channels.

*****FROM RADIOMETRIC MODEL*****				NDVI (IR-RED)/(IR+RED)	CONTRAST NDVI1/NDVI2(C-1)/(C+1)	MOD
ALT= 3000FT						
F/# = F/5.6						
FL= 28mm						
PIXEL= 9MICRON						
ATMOS= ROCH-23						
SHUTTER = 1/150						
TARGET e- = 48,100						
HAZE e- = 26,500						
GSD(in)= 11.57						
NYQUIST GRD(in)= 23.14						
WHEAT-NEW TO WHEAT-GREEN COMPARISON						
***** PREDICTED GRD(in)*****						
AIRCRAFT SPEED-> 50.0	100.0	150.0	200.0	250.0	300.0	350.0
PIXEL SMEAR-> 0.51	1.010	1.52	2.03	2.53	3.04	3.55
LENS PIXEL						
IFF LIMITED GREEN	23.14	23.14	24.39	25.71	27.27	29.16
BLUE	23.14	23.14	23.14	24.39	27.27	29.16
AVG. MEASURED LENS						
GREEN	23.26	24.39	25.71	27.27	29.16	31.49
BLUE	23.14	23.14	23.26	25.71	27.27	29.16
WHEAT-NORM TO WHEAT-GREEN COMPARISON						
***** PREDICTED GRD(in)*****						
GRD = 257.14in						
-> NOT ENOUGH CONTRAST TO DETECT A DIFFERENCE						
Q: WHAT IS THE MINIMUM ALLOABLE TARGET CONTRAST WHICH CAN BE DETECTED?						
ALT= 3000FT						
F/#= F/5.6						
FL= 28mm						
PIXEL= 9MICRON						
ATMOS= ROCH-23						
SHUTTER= 1/150						
SPEED= 100mph						
LENS= AVG. MEASURED						
A: THE MINIMUM ALLOWABLE CONTRAST TO DETECT CHANGE IS 1.0661						
->NDVI = 0.8262 (ASSUMING WHEAT-GRN AS THE REF)						
PIXEL	GRD(in)					
GREEN	257.14					
BLUE	181.83					

Table 4: Wheat Case-Study Image Quality Summary

5.0 Conclusion / Summary

The project has been very helpful on understanding the technical aspects of the CIR camera and its usefulness for remote sensing. The project's main focus of creating an analytical model of the CIR camera has been successfully accomplished. Clearly, the model can be useful to predict both radiometric and image quality camera performance in airborne applications. From the results presented, it is clear that the camera has excellent image capture capabilities for remote sensing applications. Because of the camera's unique filtering flexibility, one can only imagine the imaging possibilities. With the use of the model, one can easily predict and optimize performance before costly aerial flights occur. As presented throughout this paper, the measured data will be very useful for future analysis on other imaging research projects.

Suggestion for Future Follow-on Work

Lab and Field Radiometric Camera Calibration Testing

A better understanding of the actual camera output relative to the model's results needs to be explored. One approach, to baseline the camera's actual performance, involves the use of an integrating sphere and a calibrated blackbody light source. The light source could be easily filtered and therefore, camera output to known spectral radiance input data could be collected. The results of this valuable lab data could be incorporated into the model to incorporate the offsets and gain parameters in the color balance section of the model. Once the lab work was completed, a similar experiment could be performed outside using multiple cameras at multiple altitudes to better understand the atmospheric impacts on the camera performance.

Modeling the Current Driver V3.0.3 Interpolation

The model currently does not perform the color interpolation function that the camera software driver does. Currently, the color interpolation technique used in the driver is a Kodak proprietary algorithm. If the proprietary algorithm was incorporated into the model, it would enhance its accuracy and predictability. One could also compare the results of the data with results from using another interpolation to see if there is a better choice for interpolations when radiometric integrity of the data is essential.

Filter Study

The model could be used to design and optimize new band-pass filters based on unique detection applications. The current band-pass filter was designed for pest detection in forests. While this filter works well for other applications, it probably is not the optimal filter for every remote sensing application. Broader band passes and/or narrower band passes may yield better results for certain applications.

Measured Temporal Spectral Reflectance Data of Various Plants

Currently, the model only has wheat incorporated for temporal studies. One could easily incorporate other types of crop data into the model once the data is measured or is located. Note the model used spectral reflectance data from 400 nm to 1000 nm at 5 nm increments.

8-bit vs 12-bit vs 14-bit

The model predicts both 8-bit and 12-bit radiometric results. One could perform a study to predict the enhanced detection capabilities of the camera if 12-bit or even 14-bit data was accessible to the end user. Currently, the CIR camera does not let the end user have access to the original 12-bit. If the results of a larger dynamic range study show significant improvements for remote sensing, there may be ways to incorporate this into the camera. The modifications needed to the camera must be compared to the cost of implementing these changes to see if it is financially beneficial.

Visual Simulations

Incorporation of the CIR camera parameters into DIRSIG. This would help further validate the camera model. Also, once the camera parameters are in DIRSIG, visual simulations of the CIR camera 's output image can easily be generated. One interesting visual simulation that could be produced, is the color aliasing artifacts caused by under sampling a busy scene and the color interpolation processing¹⁵.

6.0 Appendix

Appendix 1 - Flight Test Image



Appendix 2 - NDVI Image of the Flight Test Image



Appendix 3 - Radiometric Model Sample Run

CONSTANTS:		INPUTS:		CAMERA TYPE(20 or 40)=		460		LENS FALL-OFF ENERGY FACTOR		
M =	SPECTRAL RADIANT EXITANCE @sec*cm^2*um	FIELD POINT(0.0:25.0:5.0:1.0)=	0	FIELD POINT	4.20	4.60				
E =	SPECTRAL IRRADIANCE AT THE DETECTOR (q/sec*cm^2*um)	PIXEL SIZE (um) =	9.0				1.000	1.000		
WL =	EMITTED WAVELENGTH IN (UM)	FILL FACTOR =	1				0.991	0.963		
T =	BLACKBODY TEMP IN (DEG K)	SATURATION LEVEL(e) =	8.5000				0.500	0.864		
h =	PLANCKS CONSTANT	SENSOR NOISE (e)=	2.0				0.750	0.732		
c =	SPEED OF LIGHT	FL(mm) =	2.8				1.000	0.865		
K =	JOULTMANS CONSTANT	F# =	5.6					0.594		
R _s = SUN RADIUS	1.96648E-25	T(sec) =	0.0066666667	Delta WL (um) =	0.005	460.00				
R _{es} = EARTH TO SUN DISTANCE	4.32000 MILES	ANGLE (RAD) =	0.09		1.000		ERROR			
OPTIONS FOR TARGET REFLECT		SUN ZENITH ANG(deg)=	30.00					1		
OPTIONS FOR EXOATMOS IRRAD		White								
T1		Neutral-5								
Black		Neutral-3.5								
Es-roch23		T1-roch23	SL-roch23	T2-roch23	SL-roch23					
Es-roch7		T1-roch7	SL-roch7	T2-roch7	SL-roch7					
Es-roch5+		T1-roch5+	SL-roch5+							
enter data name		enter data name	enter data name	enter data name	enter data name					
Es-roch23		T1-roch23	WHEAT-GRN	SL-roch23	T2-roch23	SL-roch23				
SIG TERM										
Exoatmos Irrad		atmos trans	Target	Atmos Trans	Upwelled Radiance	HAZE TERM				
Es(Watts/m^2*um)		SUN TO TARGET TRAN		(Watts/m^2*um^2*sr)						
Es		T1	T1-roch23	T2	T2-roch23					
Es-roch23		WHEAT-GRN	reflect	SLd-roch23	SLd-roch23					
Es(Watts/m^2*um)		(%)		(W/m^2*um^2*sr)	(W/m^2*um^2*sr)					
Wl(um)	VL(um)	6.00000	0.00216	49.6134	3.598856	2.308	38.307			
4.00	0.4	1581.88615	17.22445	50.63874	37.24891	2.054	39.889	0.00000		
4.05	0.405	1688.99866	13.61439	51.50794	28.67223	2.292	30.965	0.00000		
4.10	0.41	1374.52569	19.50719	52.50166	37.749976	3.258	40.998	0.00000		
4.15	0.415	1840.53909	20.38565	53.00000	53.73406	2.734	31.053	0.00000		
4.20	0.42	1456.55491	2.25164	54.00000	54.23776	3.093	32.046	0.00000		
4.25	0.425	1533.98834	22.1124	6.10000	55.00979	2.486	23.794	0.00000		
4.30	0.43	1162.24074	22.97714	6.10000	55.00979	21.30790	6.8780	0.00000		
4.35	0.435	1775.23665	23.87755	6.10000	55.00979	31.3982	35.531	0.00000		
4.40	0.44	1673.84008	24.84067	56.61059	28.82105	3.872	32.693	0.00000		
4.45	0.445	1928.86352	25.65499	56.00000	57.3069	4.666	36.933	0.00000		
4.50	0.45	2029.53830	26.31799	6.00000	58.15504	5.136	38.320	0.00000		
4.55	0.455	1912.25253	27.12440	6.00000	58.84287	5.053	35.338	0.00000		
4.60	0.46	1989.51150	27.92268	5.90000	59.52916	30.24482	35.394	0.00000		
4.65	0.465	1840.53963	28.70857	5.90000	0.00433	30.33887	35.393	0.00000		
4.70	0.47	1892.17001	29.51634	6.00000	60.19763	5.193	32.432	0.00000		
4.75	0.475	2003.22894	30.26349	5.80000	0.00577	60.8826	32.709	0.00000		
4.80	0.48	2022.47226	31.03440	5.80000	0.00578	61.44946	5.980	34.034	0.00000	
4.85	0.485	1857.70582	31.81434	6.00000	0.00336	62.11615	6.245	33.674	0.00000	
4.90	0.49	2032.38687	32.54966	6.00000	0.00004	62.77119	24.57103	5.929	30.500	0.00000
4.95	0.495	2032.34506	33.30139	6.00000	0.00013	63.29490	25.98790	6.810	32.798	0.00000
5.00	0.5	1843.90790	34.01442	6.00000	0.00141	64.45236	6.30229	7.036	32.337	0.00000
5.05	0.505	1823.58587	34.72745	6.10000	0.00439	64.98917	21.44779	6.934	29.009	0.00000
5.10	0.51	1872.66110	35.45733	6.30000	0.00756	61.44946	28.04047	5.980	28.382	0.00000
5.15	0.515	1764.44867	36.19233	6.40000	0.00748	66.03592	27.44924	7.583	27.743	0.00000
5.20	0.52	1797.70582	37.81434	6.60000	0.00706	66.50339	24.57103	8.060	28.696	0.00000
5.25	0.525	1879.26461	38.58319	6.70000	0.00572	67.00890	19.84476	8.772	28.617	0.00000
5.30	0.53	1836.35559	38.28319	6.90000	0.00499	67.54423	18.86692	9.058	27.925	0.00000
5.35	0.535	1809.56892	38.07669	7.00000	0.00142	68.00000	22.31888	6.690	29.009	0.00000
5.40	0.54	1718.10422	39.55670	7.00000	0.00616	68.50573	16.73435	9.036	28.382	0.00000
5.45	0.545	1883.32687	40.31451	6.00000	0.00666	68.98660	21.33686	7.583	28.920	0.00000
5.50	0.55	1824.59303	40.98805	7.00000	0.00787	69.46224	19.71809	7.472	27.190	0.00000
5.55	0.555	1847.50104	41.54434	6.90000	0.00756	69.79983	16.71849	8.060	27.049	0.00000
5.60	0.56	1778.23709	42.08217	6.70000	0.00755	70.10065	15.75167	9.058	26.945	0.00000
5.65	0.565	1838.72452	42.99315	6.50000	0.00800	70.5934	15.91264	9.931	25.844	0.00000
5.70	0.57	1788.14061	43.49071	6.20000	0.00707	70.73342	15.04993	9.324	24.374	0.00000
5.75	0.575	1787.12085	43.54940	6.00000	0.00495	71.19966	14.58859	9.180	23.879	0.00000
5.80	0.58	1789.33247	44.14199	5.70000	0.00258	71.56581	14.44625	8.888	23.334	0.00000
5.85	0.585	1686.34481	44.21366	5.60000	0.00167	71.86773	14.05426	8.667	22.333	0.00000
5.90	0.59	1668.56214	44.21366	5.30000	0.00635	71.65058	12.70420	7.743	20.498	0.00000
5.95	0.595	1728.38862	44.81757	5.10000	0.00581	71.99051	12.88113	7.862	20.714	0.00000

PIXEL OUTPUT:	MONOCHROME (red+ir)	RAW RED (red)	matrixed red (red)	RAW GREEN (green+ir)	matrixed green (green)	RAW BLUE (ir)	matrixed blue (ir)	NDVI (ir-red)/(ir+red)
SIGNAL # of e's per pixel=	48128.14	31225.44	3804.53	18338.39	4450.38	13670.57	70803.58	0.779
HAZE # of e's per pixel=	26322.93	10672.62	15332.85	7124.66	20851.43	2031.09	10674.92	-0.179
Total(SIG+HAZE) # of e's per pixel=	74551.07	41898.07	24137.38	25446.35	25301.81	15731.66	81478.50	0.543
SENSOR NOISE(e)= 20.00	20.00	20.00	20.00	20.00	20.00	20.00	20.00	0.000
SHOT NOISE(e)= 2.73.22	204.69	155.36	159.57	159.07	125.43	255.44	229.5	
12bit QUANTIZE NOISE(e)= 5.26	2.95	1.70	1.79	1.78	1.11	5.74	5.53	
8bit QUANTIZE NOISE(e)= 84.18	47.25	27.22	28.71	28.53	17.74	91.68	95.13	
Total Sensor&Elec Noise # of e's per pixel=	286.64	211.04	159.00	163.38	162.85	128.25	300.59	0.308
Grand Total # of e's per pixel=	74937.71	42109.11	24296.38	25627.22	25454.66	15859.91	81779.09	0.542
12bit constant=	20.75							
8bit constant=	16.00							
12bit counts for SIGNAL e's=	2319	1505	424	844	214	659	3412	0.779
12bit counts for HAZE e's=	1778	514	739	343	205	99	514	-0.180
Total(SIG+HAZE) # of e's=	3397	2019	1163	1227	1219	758	3936	0.543
12bit counts for TotalSensor &electronicsNoise e's=	14	10	8	8	6	14	2.23	
12bit counts for grand total e's=	3611	2029	1171	1235	1227	764	3541	0.542
8bit counts for SIGNAL e's=	145	94	27	5	5	41	213	0.775
8bit counts for HAZE e's=	80	32	46	21	63	6	32	-0.179
8bit counts for total(sig+HAZE) e's=	225	126	73	77	76	47	245	0.541
						0	1	normalized
8bit counts for TotalSensor &electronicsNoise e's=	1	1	1	1	1	0	0	0.000
								FILT
								CFA
								RED
								13-15
								CFB-B
TOTAL(SIG+HAZE) Radiance at Detector (Watts/m ² *sr)	SIGNAL Only IRRADIANCE at Detector (si-sec-m ² *um)	Q.E. Norm Factor= 0.45	MONOCHROME SIGNAL Only # of electrons # of electrons e- per delta wl	MONOCHROME SIGNAL Only # of electrons # of electrons e- per delta wl	MONOCHROME TOTAL(SIG+HAZE) # of electrons # of electrons e- per delta wl	MONOCHROME TOTAL(SIG+HAZE) # of electrons # of electrons e- per delta wl	Y91 CFA-2 WAVE	
0.00E+00	0.00E+00	0.00E+00	0.07875	0	0	0	400	0.1517
0.00E+00	0.00E+00	0.00E+00	0.18	0.081	0	0	405	0.15245
0.00E+00	0.00E+00	0.00E+00	0.185	0.0825	0	0	410	0.1132
0.00E+00	0.00E+00	0.00E+00	0.155	0.0875	0	0	415	0.1022
0.00E+00	0.00E+00	0.00E+00	0.125	0.0625	0	0	420	0.0912
0.00E+00	0.00E+00	0.00E+00	0.1325	0.05625	0	0	425	0.0865
0.00E+00	0.00E+00	0.00E+00	0.14	0.063	0	0	430	0.0818
0.00E+00	0.00E+00	0.00E+00	0.175	0.07875	0	0	435	0.07875
0.00E+00	0.00E+00	0.00E+00	0.21	0.0945	0	0	440	0.0757
0.00E+00	0.00E+00	0.00E+00	0.245	0.11025	0	0	445	0.07375
0.00E+00	0.00E+00	0.00E+00	0.28	0.126	0	0	450	0.0718
0.00E+00	0.00E+00	0.00E+00	0.3	0.135	0	0	455	0.0726
0.00E+00	0.00E+00	0.00E+00	0.32	0.144	0	0	460	0.0734
0.00E+00	0.00E+00	0.00E+00	0.31	0.1395	0	0	465	0.0777
0.00E+00	0.00E+00	0.00E+00	0.3	0.135	0	0	470	0.082
0.00E+00	0.00E+00	0.00E+00	0.295	0.13275	0	0	475	0.08985
0.00E+00	0.00E+00	0.00E+00	0.29	0.1305	0	0	480	0.0977
0.00E+00	0.00E+00	0.00E+00	0.285	0.12825	0	0	485	0.1015
0.00E+00	0.00E+00	0.00E+00	0.28	0.126	0	0	490	0.1186
0.00E+00	0.00E+00	0.00E+00	0.28	0.126	1	0	495	0.1152
0.00E+00	0.00E+00	0.00E+00	0.28	0.126	0	0	500	0.1318
5.04E-02	9.84E-16	4.03E-17	0.305	0.13725	7292	36	2984.5	505
7.56E-02	1.60E-17	6.10E-17	0.33	0.1485	12823	64	4890.5	540
6.30E-02	1.54E-17	5.62E-17	0.38	0.171	14264	71	5193.8	515
6.19E-02	1.48E-17	5.09E-17	0.43	0.1935	15482	207	5302.2	520
1.39E-01	3.55E-17	1.16E-18	0.48	0.216	41350	134985	674	525
7.50E-02	2.04E-17	6.29E-17	0.53	0.2385	26275	131	8100.5	405
7.61E-02	2.17E-17	6.32E-17	0.585	0.23825	30847	154	914.76	535
1.23E-01	3.69E-17	1.05E-18	0.64	0.288	57369	287	16316.6	818
1.72E-01	5.35E-17	1.49E-18	0.69	0.3105	69638	447	249140	540
1.63E-01	5.29E-17	1.41E-18	0.74	0.333	94611	473	254432	550
1.65E-01	1.45E-18	0.795	0.35775	106287	531	280054	1400	0.0782
1.53E-01	5.16E-17	1.35E-18	0.85	0.3825	106533	533	279006	405
1.44E-01	4.94E-17	1.29E-18	0.885	0.39825	106310	532	276345	183
1.28E-01	4.43E-17	1.13E-18	0.92	0.414	99080	495	25893.3	570
1.25E-01	4.36E-17	1.06E-18	0.925	0.41625	98026	490	25497.6	540
1.26E-01	4.40E-17	1.16E-18	0.93	0.4185	99448	497	261388	580
1.28E-01	4.55E-17	1.19E-18	0.925	0.41625	10176	509	266336	585
1.18E-01	4.16E-17	1.10E-18	0.92	0.414	93039	465	263335	590
1.19E-01	4.25E-17	1.12E-18	0.925	0.41625	95459	477	251440	595

		normalized				normalized				normalized				normalized			
		FILT	CFA	BLUE	CFA	RED Pixel	RED Pixel	GREEN Pixel	GREEN Pixel	BLUE Pixel	BLUE Pixel	SIGNAL Only	TOTAL(SIG+H)	SIGNAL Only	TOTAL(SIG+H)		
		FILT	CFA	BLUE	CFA	SIGNAL Only	TOTAL(SIG+HAZE)	SIGNAL Only	TOTAL(SIG+HAZE)	SIGNAL Only	TOTAL(SIG+H)	# of electrons	# of electrons	# of electrons	# of electrons		
						# of electrons	# of electrons	# of electrons	# of electrons	# of electrons	# of electrons	# of e- at wl					
						e- per deltawl	e- per deltawl	e- per deltawl	e- per deltawl	e- per deltawl	e- per deltawl	# of e- at wl					
						0.1042	0.4335	0	0	0	0	0	0	0	0	0	
						0.09975	0.4909	0	0	0	0	0	0	0	0	0	
						0.0983	0.5463	0	0	0	0	0	0	0	0	0	
						0.0991	0.5796	0	0	0	0	0	0	0	0	0	
						0.0849	0.6109	0	0	0	0	0	0	0	0	0	
						0.0833	0.629	0	0	0	0	0	0	0	0	0	
						0.0817	0.6471	0	0	0	0	0	0	0	0	0	
						0.08075	0.66005	0	0	0	0	0	0	0	0	0	
						0.0798	0.6733	0	0	0	0	0	0	0	0	0	
						0.0796	0.67375	0	0	0	0	0	0	0	0	0	
						0.0794	0.6745	0	0	0	0	0	0	0	0	0	
						0.08355	0.6808	0	0	0	0	0	0	0	0	0	
						0.0877	0.6471	0	0	0	0	0	0	0	0	0	
						0.09955	0.6106	0	0	0	0	0	0	0	0	0	
						0.1114	0.5741	0	0	0	0	0	0	0	0	0	
						0.1364	0.51875	0	0	0	0	0	0	0	0	0	
						0.1614	0.4634	0	0	0	0	0	0	0	0	0	
						0.2131	0.3984	0	0	0	0	0	0	0	0	0	
						0.2648	0.3394	0	0	0	0	0	0	0	0	0	
						0.34955	0.27535	0	0	0	0	0	0	0	0	0	
						0.4345	0.2173	0	0	0	0	0	0	0	0	0	
						0.5206	0.1753	726	4	2973	15	3037	15	12430	62	1033	5
						0.6067	0.1333	1202	6	4585	23	6224	31	23737	119	1337	7
						0.6606	0.1068	1170	6	4259	21	7538	38	27432	137	1219	6
						0.673	0.0803	1089	5	3741	19	6849	44	30410	152	995	5
						0.7219	0.06805	2587	13	6439	42	24079	120	78552	393	2185	11
						0.7413	0.0518	1440	7	4439	22	15582	78	48039	240	1059	5
						0.73285	0.04735	1683	8	4991	25	18085	90	53831	268	1168	6
						0.7244	0.0429	3116	16	8888	44	33247	166	94819	474	1949	10
						0.6987	0.0411	5390	25	14141	71	50121	251	139260	696	2948	15
						0.673	0.0393	5601	28	15062	75	50939	255	136886	685	2975	15
						0.6289	0.0343	6126	31	16142	81	52475	267	140001	705	2917	15
						0.5848	0.0293	5978	30	15647	78	49869	249	130530	653	2499	12
						0.53955	0.02465	5956	28	14118	74	45587	229	11941	597	2036	10
						0.4943	0.02	4985	25	13331	65	39172	196	10240	512	1515	8
						0.4546	0.0198	5388	27	14014	70	33650	178	92730	464	1513	8
						0.4149	0.0196	5927	30	15561	78	33009	165	86660	433	1519	8
						0.3734	0.02625	8171	44	29852	114	30406	152	79709	399	2138	11
						0.3319	0.0293	1093	52	27511	138	24709	124	6507	327	2449	12
						0.2751	0.04255	16858	84	44414	222	21004	105	53377	277	3249	16

6.0	0.6	1727.67411	4.5.96223	5.00000	0.00488	72.70737	12.72146	7.916	20.597	79.27554	92.279	4.61E-02
6.05	0.605	1737.45111	4.6.66173	5.00000	0.00711	73.12085	12.55669	8.192	20.558	81.99533	92.447	4.91E-02
6.10	0.61	1676.86226	4.7.11244	5.00000	0.00791	73.42241	11.85093	8.025	18.976	84.735	92.583	4.98E-02
6.15	0.615	1657.61145	4.7.55567	5.10000	0.00826	73.7205	11.50038	8.207	19.708	82.896	92.838	5.08E-02
6.20	0.62	1657.05252	4.8.04917	5.20000	0.00832	74.01807	11.25760	8.480	19.717	84.414	93.039	5.08E-02
6.25	0.625	1610.15936	4.8.59966	5.40000	0.00857	74.31041	10.67453	8.674	19.448	79.583	93.135	5.08E-02
6.30	0.63	1627.51147	4.8.88710	5.50000	0.00837	74.53565	10.55615	9.026	19.882	80.31882	93.281	5.35E-02
6.35	0.635	1619.34040	4.9.35774	5.70000	0.00712	74.83228	10.31617	9.431	19.147	82.23457	93.419	5.19E-02
6.40	0.64	1540.42875	4.9.86025	5.80000	0.00713	75.13190	9.61892	9.257	18.776	82.80900	93.521	5.17E-02
6.45	0.645	1552.69114	5.0.13640	5.90000	0.00727	75.31066	9.46997	9.567	19.037	80.83708	93.635	5.73E-02
6.50	0.65	1505.22776	5.0.14350	6.00000	0.00845	75.51316	9.49616	9.442	18.389	78.25389	94.545	5.48E-02
6.55	0.655	1538.22771	5.0.73771	6.00000	0.00810	75.68482	8.97325	9.807	18.180	77.47328	93.737	6.37E-02
6.60	0.66	1487.50512	5.1.54191	6.00000	0.00813	76.05149	8.58559	9.695	18.280	78.50149	93.710	5.34E-02
6.65	0.665	1494.61483	5.2.08133	6.10000	0.00814	76.47736	8.47998	10.034	16.528	79.7734	93.498	5.04E-02
6.70	0.67	1492.43731	5.2.55093	6.20000	0.00853	76.74432	8.26409	10.324	18.588	79.12924	93.498	6.04E-02
6.75	0.675	1470.44829	5.2.91034	6.30000	0.00866	76.70448	7.98849	10.790	18.779	76.0755	93.388	6.06E-02
6.80	0.68	1448.83434	5.3.39776	6.40000	0.00828	77.05591	7.74169	11.410	19.152	71.66328	93.253	6.03E-02
6.85	0.685	1434.91668	5.7.57943	6.50000	0.00824	77.48331	7.47991	12.407	19.887	67.88081	93.065	6.18E-02
6.90	0.69	1423.92231	5.4.04648	6.80000	0.00844	77.66886	7.30888	13.906	21.215	64.40806	92.713	5.63E-02
6.95	0.695	1391.15656	5.2.57141	9.50000	0.00827	76.83770	6.79007	14.777	21.567	61.85288	92.484	6.69E-02
7.00	0.705	1365.21055	7.0.28117	11.00000	0.00749	77.24778	6.59138	20.693	59.41877	7.40E-02		
7.05	0.705	1376.70130	54.23398	13.00000	0.00651	77.79667	6.61892	20.884	25.053	57.16548	91.724	8.66E-02
7.10	0.71	1358.70089	56.9332	15.00000	0.00580	78.22076	6.48635	24.232	30.519	55.06519	91.236	9.63E-02
7.15	0.715	1310.48383	54.13639	17.00000	0.00492	77.52050	6.02431	25.915	31.939	53.86139	90.792	1.00E-01
7.20	0.72	1298.13184	46.70187	20.00000	0.00829	73.47956	5.61698	24.682	28.851	54.25857	90.265	9.56E-02
7.25	0.725	1308.82306	48.31415	23.00000	0.00858	74.46165	5.26953	30.019	32.288	56.86705	89.694	1.21E-01
7.30	0.73	1289.07834	51.22789	25.00000	0.00794	76.12154	5.32894	34.797	40.126	61.03524	89.169	1.50E-01
7.35	0.735	1247.70455	52.54528	28.00000	0.00757	78.05163	5.52523	43.084	48.637	64.26401	88.489	1.94E-01
7.40	0.74	1247.68456	56.64651	30.00000	0.00757	79.14986	5.42327	46.423	51.846	63.85611	87.877	2.06E-01
7.45	0.745	1230.43352	57.42871	32.00000	0.00708	79.57933	5.31468	49.786	55.101	60.24215	87.175	2.07E-01
7.50	0.75	1210.55158	57.64010	34.00000	0.00805	79.61568	5.17295	52.496	57.669	57.48181	86.473	2.06E-01
7.55	0.755	1229.67776	58.01514	35.00000	0.00806	79.92494	5.15728	55.273	60.430	66.46102	85.806	2.12E-01
7.60	0.76	1211.81925	58.32761	37.00000	0.00780	80.20704	5.02039	57.965	62.986	52.91744	85.002	2.06E-01
7.65	0.765	1190.90381	58.59603	37.00000	0.00820	80.24266	4.85246	57.346	62.199	43.61011	84.208	1.67E-01
7.70	0.77	1172.11416	58.68822	38.00000	0.00775	80.37479	4.72219	58.321	60.043	36.30558	83.415	1.40E-01
7.75	0.775	1127.01785	59.11979	38.00000	0.00775	80.51231	4.46167	56.439	57.720	40.68622	82.679	1.48E-01
7.80	0.78	1145.53852	59.31644	38.00000	0.00805	80.66318	4.47039	50.344	56.190	30.06956	81.908	1.12E-01
7.85	0.785	1148.81080	59.52523	38.00000	0.00823	80.78020	4.42985	58.121	61.551	47.702	81.028	1.78E-02
7.90	0.79	1135.94615	59.22125	38.00000	0.00834	80.62333	3.91621	57.121	61.398	60.157	80.893	3.08E-03
7.95	0.795	1083.71172	59.55952	38.00000	0.00743	80.80555	4.03433	54.896	59.930	0.21000	79.223	7.22E-04
8.00	0.8	1090.53775	59.83049	38.00000	0.00743	81.09493	3.99868	55.546	55.546	0.00500	78.404	1.86E-04
8.05	0.805	1066.213105	60.23045	38.00000	0.00801	81.15911	3.87300	54.858	55.731	0.00334	77.538	1.12E-05
8.10	0.81	1068.34815	60.14277	38.00000	0.00805	81.14163	3.81009	54.844	56.654	0.00000	76.855	2.00E-00
8.15	0.815	1076.33474	56.23004	38.00000	0.00770	79.04162	3.55222	50.344	55.896	0.00000	76.012	3.00E+00
8.20	0.82	1027.57784	55.81138	37.00000	0.00770	78.8899	3.21621	46.419	47.735	0.00000	75.106	4.00E+00
8.25	0.825	1038.66545	57.03001	37.00000	0.00792	79.57983	3.06438	48.284	50.658	0.00000	74.452	5.00E+00
8.30	0.83	1031.93447	58.01388	37.00000	0.00645	80.05714	3.33838	49.128	52.467	0.00000	73.617	6.00E+00
8.35	0.835	1012.50106	60.63774	37.00000	0.00645	81.47736	3.30568	51.204	55.560	0.00000	72.733	7.00E+00
8.40	0.84	1006.15130	61.62931	37.00000	0.00819	81.93448	3.30202	52.216	55.546	0.00000	72.079	8.00E+00
8.45	0.845	997.07910	62.38684	37.00000	0.00800	82.32340	3.27682	52.413	56.750	0.00000	71.284	9.00E+00
8.50	0.85	902.45454	62.63635	37.00000	0.00558	82.64546	3.00633	47.727	50.632	0.00000	70.610	1.00E+00
8.55	0.855	906.70750	63.30286	37.00000	0.00558	82.97126	3.00686	40.051	42.500	0.00000	69.756	2.00E+00
8.60	0.86	922.24033	64.22033	37.00000	0.00780	82.97601	2.96677	51.683	55.134	0.02661	69.886	7.66E-05
8.65	0.865	955.51125	63.62615	37.00000	0.00752	82.97052	2.90650	50.506	56.650	0.02103	67.751	5.82E-05
8.70	0.87	939.27618	63.83359	37.00000	0.00752	83.03976	2.90634	51.065	55.972	0.12443	67.984	3.39E-04
8.75	0.875	924.65378	64.06292	37.00000	0.00751	83.21306	2.92098	50.507	57.500	0.00000	67.532	2.29E-04
8.80	0.88	938.70871	64.22033	37.00000	0.00671	83.30224	2.82775	51.427	54.255	0.13070	67.750	2.44E-04
8.85	0.885	931.94112	65.81131	37.00000	0.00674	83.4145	2.87578	51.137	54.894	0.00303	64.263	1.01E-04
8.90	0.89	922.76802	54.51864	37.00000	0.00782	83.11955	2.67619	50.213	52.889	0.05116	62.250	1.38E-04
8.95	0.895	839.32533	23.31238	37.00000	0.00755	56.35223	0.92488	43.104	45.788	0.11435	63.881	1.93E-04
9.00	0.9	895.21553	4.02381	37.00000	0.00752	74.20462	0.29987	32.387	34.300	0.12005	63.917	2.11E-04
9.05	0.905	902.13625	50.11440	37.00000	0.00639	40.9288	0.46170	37.456	39.532	0.00000	63.500	0.00E+00
9.10	0.91	882.13625	51.71365	37.00000	0.00636	76.71658	1.94673	35.363	37.810	0.13070	62.750	2.29E-04
9.15	0.915	881.40282	51.71365	37.00000	0.00636	79.41466	1.94646	35.944	37.810	0.13070	62.750	2.44E-04
9.20	0.92	865.94112	51.58045	37.00000	0.00636	78.42107	1.94646	35.944	37.810	0.13070	62.750	2.44E-04
9.25	0.925	898.07500	51.95112	37.00000	0.00784	80.01395	1.94646	35.944	37.810	0.13070	62.750	2.44E-04
9.30	0.93	892.76814	63.83407	37.00000	0.00782	80.11715	2.38423	41.404	45.788	0.11435	62.750	2.44E-04
9.35	0.935	834.94723	4.02381	37.00000	0.00639	1.91341	0.46170	34.300	36.352	0.00000	63.500	0.00E+00
9.40	0.94	831.56152	9.87045	37.00000	0.00639	40.9288	1.94636	33.610	35.494	0.13666	63.000	2.29E-04
9.45	0.945	810.65197	8.83115	37.00000	0.0							

1.20E-01	4.39E+17	1.14E+18	0.93	0.4185	98952	495	256787	1284	600	0.302
1.24E-01	4.70E+17	1.19E+18	0.935	0.42075	108761	544	270541	1333	605	0.408
1.23E-01	4.80E+17	1.19E+18	0.94	0.423	108714	549	271741	1339	610	0.514
1.22E-01	4.94E+17	1.19E+18	0.91	0.4095	109297	546	263449	1312	615	0.5974
1.18E-01	4.95E+17	1.16E+18	0.88	0.396	106514	533	247671	1238	620	0.6808
1.13E-01	5.03E+17	1.12E+18	0.83	0.3735	101364	507	226111	1131	625	0.73755
1.16E-01	5.33E+17	1.16E+18	0.78	0.351	101003	505	219127	1096	630	0.7943
1.20E-01	5.75E+17	1.20E+18	0.75	0.3375	105571	528	221054	1105	635	0.82665
1.16E-01	5.74E+17	1.17E+18	0.73	0.3285	101805	519	20552	1038	640	0.859
1.14E-01	5.89E+17	1.16E+18	0.725	0.3225	105927	515	204806	1024	645	0.8795
1.07E-01	5.63E+17	1.10E+18	0.72	0.324	98522	493	191866	939	650	0.8895
1.08E-01	5.83E+17	1.12E+18	0.75	0.3375	106333	532	203626	1018	655	0.90785
1.06E-01	5.89E+17	1.11E+18	0.78	0.351	111587	558	210407	1052	660	0.9162
1.09E-01	6.24E+17	1.15E+18	0.815	0.36675	123641	618	227915	1140	665	0.92045
1.09E-01	6.40E+17	1.15E+18	0.85	0.3925	132209	661	238041	1190	670	0.9247
1.08E-01	6.44E+17	1.16E+18	0.875	0.3975	131634	688	239496	1197	675	0.9279
1.01E-01	6.49E+17	1.09E+18	0.9	0.405	141835	709	238070	1190	680	0.9311
9.91E-02	6.70E+17	1.07E+18	0.9	0.405	144340	732	234712	1174	685	0.9315
1.00E-01	7.17E+17	1.09E+18	0.9	0.405	156731	734	239109	1196	690	0.9332
9.76E-02	7.36E+17	1.07E+18	0.975	0.39975	156237	781	228030	1140	695	0.9343
1.03E-01	8.16E+17	1.14E+18	0.85	0.3625	161247	700	23478	1172	700	0.9354
1.14E-01	9.68E+17	1.27E+18	0.815	0.3675	191236	956	251846	1259	705	0.93755
1.22E-01	1.08E+18	1.37E+18	0.78	0.361	204885	1024	259727	1299	710	0.9397
1.24E-01	1.13E+18	1.40E+18	0.755	0.33875	207928	1040	256225	1281	715	0.94295
1.16E-01	1.09E+18	1.32E+18	0.73	0.3285	193114	969	233559	1118	720	0.9462
1.42E-01	1.39E+18	1.63E+18	0.72	0.324	243918	1215	285659	1438	725	0.9517
1.73E-01	1.73E+18	1.98E+18	0.71	0.3195	298335	1492	344233	1720	730	0.9572
2.19E-01	2.25E+18	0.725	0.3225	398815	1934	447955	2240	735	0.9605	
2.30E-01	2.44E+18	2.66E+18	0.74	0.333	433590	2168	484243	2421	740	0.96338
2.28E-01	2.44E+18	2.70E+18	0.77	0.3465	458869	2279	504533	2523	745	0.96715
2.26E-01	2.45E+18	2.69E+18	0.8	0.36	475338	2377	522718	2611	750	0.9705
2.32E-01	2.53E+18	2.76E+18	0.84	0.378	516169	2581	564331	2822	755	0.97385
2.24E-01	2.48E+18	2.69E+18	0.88	0.396	530010	2650	575915	2890	760	0.9772
1.81E-01	2.02E+18	2.19E+18	0.91	0.4095	445595	2228	483300	2417	765	0.98285
1.51E-01	2.41E+18	2.66E+18	0.94	0.423	388558	1913	420019	2100	770	0.9885
1.68E-01	1.86E+18	1.96E+18	0.96	0.432	422991	2115	456830	2222	775	0.99195
1.21E-01	1.39E+18	1.48E+18	0.98	0.441	332051	1651	353865	1779	780	0.9954
3.91E-02	2.21E+17	2.70E+17	0.99	0.4455	53063	265	57108	286	785	0.9955
3.31E-03	3.88E+16	4.14E+16	1	0.45	9351	47	10051	50	790	0.9977
7.75E-04	9.09E+15	9.75E+15	0.98	0.441	2163	11	232	12	795	0.99885
1.99E-04	2.39E+15	2.56E+15	0.96	0.432	548	3	587	3	800	1
1.20E-05	1.43E+14	1.58E+14	0.94	0.423	33	0	35	0	805	1
0.00E+00	0.00E+00	0.00E+00	0.92	0.414	0	0	0	0	810	1
0.00E+00	0.00E+00	0.00E+00	0.88	0.396	0	0	0	0	815	1
0.00E+00	0.00E+00	0.00E+00	0.84	0.378	0	0	0	0	820	1
0.00E+00	0.00E+00	0.00E+00	0.835	0.3775	0	0	0	0	825	1
0.00E+00	0.00E+00	0.00E+00	0.83	0.3735	0	0	0	0	830	1
0.00E+00	0.00E+00	0.00E+00	0.83	0.3735	0	0	0	0	835	1
0.00E+00	0.00E+00	0.00E+00	0.83	0.3735	0	0	0	0	840	1
0.00E+00	0.00E+00	0.00E+00	0.825	0.37125	0	0	0	0	845	1
0.00E+00	0.00E+00	0.00E+00	0.82	0.369	0	0	0	0	850	1
0.00E+00	0.00E+00	0.00E+00	0.82	0.369	0	0	0	0	855	1
8.11E-05	1.10E+15	1.10E+15	0.82	0.369	208	1	220	23	860	1
6.16E-05	7.97E+14	8.42E+14	0.825	0.37125	160	1	169	1	865	1
3.56E-04	4.66E+15	4.93E+15	0.83	0.3735	940	5	904	5	870	1
0.00E+00	0.00E+00	0.00E+00	0.835	0.37575	0	0	0	0	875	1
1.92E-04	2.55E+15	2.67E+15	0.84	0.378	516	3	545	3	880	1
8.29E-06	1.10E+14	1.16E+14	0.83	0.3735	22	0	23	0	885	1
1.38E-04	1.88E+15	1.98E+15	0.82	0.369	369	1	308	2	890	1
2.09E-04	2.85E+15	3.71E+15	0.795	0.35775	680	3	738	2	900	1
2.24E-04	3.01E+15	3.19E+15	0.77	0.34665	563	3	717	4	900	1
4.61E-05	6.06E+14	6.88E+14	0.735	0.33075	72	0	82	0	905	1
0.00E+00	0.00E+00	0.00E+00	0.735	0.315	560	3	532	3	910	1
2.42E-04	3.29E+15	3.48E+15	0.7	0.315	570	3	601	3	915	1
2.57E-04	3.53E+15	3.72E+15	0.665	0.29925	225	1	226	1	920	1
1.06E-04	1.47E+15	1.54E+15	0.63	0.2835	293	1	308	2	925	1
1.46E-04	2.09E+15	2.13E+15	0.595	0.26775	387	2	419	2	930	1
1.38E-04	1.88E+15	1.94E+15	0.56	0.252	0	0	0	0	935	1
2.62E-04	3.52E+15	3.71E+15	0.525	0.2325	0	0	0	0	940	1
1.13E-06	1.30E+13	1.66E+13	0.525	0.2205	72	0	82	0	945	1
4.61E-05	6.06E+14	6.88E+14	0.49	0.2205	0	0	0	0	950	1
3.28E-05	4.47E+14	4.94E+14	0.455	0.20475	0	0	0	0	955	1
0.00E+00	0.00E+00	0.00E+00	0.42	0.189	46	0	50	0	960	1
9.71E-05	1.40E+15	1.47E+15	0.395	0.17775	0	0	0	0	965	1
0.00E+00	0.00E+00	0.00E+00	0.37	0.1665	126	1	133	1	970	1
0.00E+00	0.00E+00	0.00E+00	0.345	0.15525	0	0	0	0	975	1

INPUT DATA FILES:

705	1376.091299	54.2639822	0.006514259	77.7966708	6.618919	1372.66	2.75098	0.004216593	20.7924	7.15937	1372.66	10.4535
710	1358.700891	54.1993245	0.006800058	78.206765	6.4463448	1344.64	2.90616	0.003710527	21.74744	7.44872	1344.64	11.0902
715	1310.433828	54.1369319	0.006924318	77.750051	6.0204114	1326.17	2.69244	0.003110921	20.3333	6.56893	1326.17	10.3124
720	1288.131836	46.7018635	0.008282125	73.479363	5.16981	1285.02	1.48054	0.005354783	11.387	3.12289	1288.02	5.52042
725	1308.83058	48.3414516	0.008581391	74.46164495	5.26935	1305.68	1.56623	0.00552152	12.7168	3.37066	1305.68	6.04974
730	1289.078343	51.222789145	0.007932738	76.1275381	1285.97	1.395324	0.00582669	14.912	4.12209	1285.97	7.73304	
735	1282.704548	55.28228395	0.007647844	78.4565636	5.55234	1270.59	2.75549	0.004865798	20.2836	6.00559	1270.59	10.8511
740	1247.188477	56.8446305	0.005563625	79.1498331	4.43366	1229.27	3.36881	0.004783296	23.3773	7.33318	1229.27	13.1422
745	1230.463557	57.42818665	0.007087258	79.57831	5.14690	1243.96	3.66932	0.00420424	25.2649	8.15678	1243.96	14.4198
750	1210.515887	57.7840146	0.008050138	79.745337	5.17245	1222.27	3.75254	0.005057558	25.5113	8.18658	1222.27	14.813
755	1239.617776	58.02271545	0.008064294	79.9249355	5.17279	1205.4	3.59314	0.005454721	22.1942	6.84774	1205.4	14.2436
760	1211.819252	58.322761225	0.007895086	80.0780395	5.020394	1205.51	2.49996	0.004927611	16.3471	4.42174	1205.51	9.68394
765	1190.903805	58.89503285	0.008204333	80.22874495	4.852463	1169.17	3.82303	0.005098979	25.1885	7.44758	1169.17	15.3022
770	1172.114159	58.65222475	0.007745095	80.7374825	4.72247	1157.14	3.91394	0.00459733	25.3509	7.50797	1157.14	15.7404
775	1127.071854	59.1197938	0.007745095	80.8203195	4.451673	1157.14	3.91394	0.0047833	25.38509	7.50797	1157.14	15.7404
780	1145.538517	59.3744224	0.008050135	80.86315615	4.470394	1145.57	3.66932	0.00461631	17.0019	7.33959	1145.57	15.92
785	1148.84048	59.54523075	0.008234668	80.6253345	4.429052	1141.05	3.50568	0.005047501	23.5125	6.00579	1141.05	14.2358
790	1135.946145	59.21251522	0.008434895	80.7804577	4.472232	1101.95	3.56687	0.00508621	23.7959	5.90446	1101.95	14.5566
795	1083.731723	59.59531965	0.0074242061	80.8045477	4.0344330	1101.95	3.56687	0.00508621	23.7959	5.90446	1101.95	13.7855
800	1090.93775	59.93504927	0.0074241061	80.93942285	3.999880	1107.24	3.38007	0.004503881	22.5353	5.34094	1107.24	13.7825
805	1066.231047	60.24545135	0.008054824	81.08011282	3.810986	1080.98	3.61886	0.004833256	24.1455	7.66971	1080.98	14.9207
810	1088.381047	60.4277335	0.008054364	81.1144233	3.810986	1078.55	2.65115	0.004833298	17.0019	3.61691	1077.55	10.9847
815	1076.35474	56.5820354	0.007075524	81.2071533	3.522123	1044.57	2.99582	0.004598556	17.08335	3.34676	1045.03	10.4754
820	1027.577838	55.87137835	0.007703554	78.88599355	3.316206	1044.57	2.5132	0.004598556	17.08335	3.34676	1045.03	10.4754
825	1038.605076	57.050076	0.007919388	79.5198562	3.394477	1049.41	2.67893	0.004510123	18.3569	3.64043	1041.03	11.2223
830	1031.93445	58.07138813	0.008644785	80.30715885	3.358179	1013.73	3.37609	0.003810175	21.5468	4.44075	1101.03	14.2249
835	1012.501056	60.6677443	0.008447885	81.4713009	3.353882	1008.31	3.87881	0.004758861	24.7414	5.2697	1101.03	16.4328
840	1006.151304	61.7629081	0.008093642	81.9984755	3.823019	952.314	3.87881	0.004832851	24.7414	5.2697	1101.03	16.4328
845	997.0707045	62.3683645	0.008093641	82.32040405	3.2326119	952.314	4.15342	0.004832929	26.2403	5.32022	952.02	17.6953
850	902.345394	62.6683546	0.009575894	82.4646554	2.806627	906.241	4.23287	0.003246728	26.7196	5.22866	906.02	18.3536
855	750.9305973	63.0026355	0.005576934	82.845458	2.806627	906.241	4.23287	0.003246728	26.7196	5.22866	906.02	18.3536
860	63.63696145	63.0798175	0.007798175	82.8326735	3.068863	967.81	4.46675	0.004517881	27.3999	5.70932	968.02	19.2541
865	985.52249	63.6261523	0.007518328	74.20651045	2.966165	954.63	4.52441	0.004334659	27.48486	5.60706	954.63	9.55412
870	939.722722	63.65558575	0.007518328	83.09876025	2.9066240	954.63	4.52441	0.004334659	27.48486	5.60706	954.63	9.55412
875	924.6537796	64.0629292	0.007510409	83.21300611	2.8209778	935.938	4.52304	0.00430975	27.5012	5.42772	935.02	19.7334
880	935.7070787	64.2203401	0.006712075	83.3747417	2.8272416	933.867	4.48281	0.003832561	26.3223	5.05652	924.02	19.4396
885	931.9613074	64.2335346	0.006712075	83.474517	2.81456125	926.192	4.48281	0.003832561	26.3223	5.05652	924.02	19.4396
890	922.78114	64.5406573	0.007820072	82.845458	2.81456125	904.78	3.56632	0.004444441	21.0476	3.54717	905.02	8.57339
895	908.7542137	58.1160873	0.007223444	80.171535	3.384423	876.771	1.92681	0.004261147	13.2454	1.71612	877.02	8.77339
900	902.107024	47.45947435	0.007223444	74.20651045	1.91308	877.771	1.92681	0.004086188	13.2454	1.71612	877.02	8.77339
905	821.5615165	52.4422662	0.005992014	80.1882775	2.071551	838.566	1.87085	0.003936106	12.3665	1.53636	83.9502	8.37336
910	862.132488	50.1142215	0.005992014	75.8243412	1.883359	83.9538	1.87085	0.003936106	12.3665	1.53636	83.9502	8.37336
915	841.408164	51.716154	0.006712075	72.757384	1.94630	923.867	2.93508	0.003919127	14.3366	2.92481	924.02	19.4396
920	865.44112	56.58044815	0.006738964	78.4814755	2.03149	803.52	1.91865	0.004261147	11.9105	1.39961	80.3502	8.69668
925	829.75275486	54.51964005	0.006623024	78.42207235	1.868119	803.252	1.91865	0.004261147	11.9105	1.39961	80.3502	8.69668
930	835.3233347	53.0713839	0.00739466	75.3523115	1.924476	783.588	0.043123	0.004194792	0.5703057	0.069824	7.84102	0.197225
935	834.9421333	58.03331595	0.00739466	80.32304435	1.583437	759.04	2.46444	0.004043607	15.8153	1.64032	7.395402	11.5625
940	821.5615165	9.87044733	0.00707259	40.94284844	1.46104	770.802	0.0719309	0.00409604	1.53321	0.15867	7.715402	16.461
945	810.6509695	8.83114524	0.007408844	39.04616888	0.579446	740.985	0.30585	0.003912449	1.83261	0.15867	7.715402	16.461
950	809.893358	14.1749535	0.00118445	46.72129005	0.8362620	742.662	1.12649	0.003828807	2.70992	0.21841	7.41E+02	8.69668
955	784.991225	56.27275548	0.006623024	56.27275548	1.204311	742.662	1.12649	0.003828807	2.70992	0.21841	7.41E+02	8.69668
960	776.7327595	54.1950735	0.00739466	75.3523115	1.39576	759.04	2.46444	0.004043607	15.8153	1.64032	7.395402	11.5625
965	731.98558	68.92323295	0.006832929	85.777992	1.669551	736.418	3.47275	0.003842445	2.2934	2.2934	7.395402	23.5459
970	731.2219005	69.5274979	0.0007621118	86.0715747	1.646459	721.47	5.08678	0.003640199	28.721	3.4443	7.395402	23.5459
975	731.2219005	69.75544605	0.0067621118	86.1840606	1.609339	721.47	5.08678	0.003640199	28.721	3.4443	7.395402	23.5459
980	751.694223	67.01663965	0.006832929	84.84671115	1.61353	739.49	3.47275	0.003842445	2.2934	2.2934	7.395402	16.461
985	744.089836	67.01663965	0.006832929	84.84671115	1.61353	736.418	4.93093	0.003894059	27.6681	3.44661	7.395402	23.5459
990	731.98558	68.92323295	0.006832929	85.777992	1.669551	736.418	4.93093	0.003894059	27.6681	3.44661	7.395402	23.5459
995	731.2219005	69.5274979	0.0007621118	86.0715747	1.646459	721.47	5.08678	0.003640199	28.721	3.4443	7.395402	23.5459
1000	724.9275	69.75544605	0.0067621118	86.1840606	1.609339	721.47	5.08678	0.003640199	28.721	3.4443	7.395402	23.5459

0.01057812	36.3111	12.6603	57.16547966	0.7992226761	88.50	87.14	32.1000	75.7400	10.7800	29.2400	
0.00931764	38.2944	13.4444	55.65010049	0.69557097	88.43	88.14	33.5500	77.4900	10.7900	32.6400	
0.00793171	35.6374	11.2332	53.86133154	0.531095533	88.50	87.35	35.2800	79.0700	10.7000	35.1200	
0.01332684	21.0415	4.0885	51.58810198	0.488615036	88.33	79.06	80.3700	80.7100	10.7100	36.7800	
0.01372597	22.3596	4.47042	56.86705112	0.35485527	88.26	65.36	39.7500	81.5700	10.7000	37.8300	
0.01267848	26.2862	5.94477	61.03325162	0.249457359	88.07	54.22	42.2400	82.5800	10.7000	38.5800	
0.01215805	35.7907	10.2125	64.26010118	0.141239166	88.05	48.31	44.7100	83.3800	10.7000	39.0800	
0.01198896	41.855	13.6629	63.8584137	0.078320563	87.86	44.25	47.1400	84.0500	10.7100	39.4800	
0.01118589	44.7433	15.876	60.42574876	0.056394504	87.88	36.26	48.3600	85.6800	10.7600	39.8700	
0.01270642	45.264	15.138	57.41560887	0.0404455791	87.87	24.59	49.5000	85.0400	10.8000	40.1900	
0.0128883	39.4498	12.8938	56.461024381	0.035119057	87.69	15.24	50.3800	85.3900	10.8000	40.5100	
0.01235507	29.1166	6.9498	52.91702123	0.0501519427	87.56	10.04	54.7800	85.7400	10.8100	40.8100	
0.01282838	45.4456	14.2288	43.6103105	0.029990904	87.43	7.53	55.7100	85.9300	10.9100	41.1500	
0.01202098	46.4026	36.3098	36.3058095	0.069308281	87.30	6.48	56.1200	86.1100	10.9600	41.4800	
0.01201098	46.4026	40.0822159	0.0686684551	0.04989106	87.36	6.31	56.3100	86.2200	11.0300	41.8000	
0.01226662	46.4026	14.4438	46.6197	0.047445297	87.19	6.64	56.2600	86.4000	11.1100	42.1300	
0.01274073	42.2129	10.8121	4.770207405	0.0098942055	87.01	6.55	56.0400	86.5100	11.1900	42.4900	
0.01285751	42.8108	10.6227	0.85028123	-0.013229915	87.12	5.31	55.6500	86.5200	11.2500	42.8200	
0.01198017	33.3876	5.5334	9.2381	0.012813339	86.98	3.64	55.1600	86.5400	11.3400	43.1000	
0.01138894	40.8419	40.8419	0.053585757	-0.016403198	86.78	2.44	54.7300	86.5900	11.4400	43.4500	
0.01138894	40.8419	9.2381	43.6553	0.030333786	86.65	1.73	54.2200	86.6500	11.5600	43.7400	
0.01226662	30.7638	5.31015	0	-0.019958635	86.34	1.39	53.7600	86.7500	11.6200	44.1000	
0.01228411	31.0025	4.96006	30.69281588	0	0.000739698	86.67	1.27	53.2500	86.8400	11.7600	44.4100
0.01163376	31.0025	4.96006	0	0.069284439	86.51	1.31	52.8100	86.8200	11.8400	44.7700	
0.01198017	33.3876	5.5334	0	0.172710419	86.31	1.55	52.5500	86.8400	11.9800	45.0800	
0.010970379	39.2812	7.2327	0	0.459074974	86.08	2.04	52.1300	86.7200	12.0400	45.3900	
0.01213456	45.2096	9.10112	0	0.279140472	86.06	2.85	51.8900	86.9400	12.1600	45.6800	
0.01213456	45.2096	9.10112	0	0.044441223	85.91	3.44	51.7000	86.8900	12.2300	45.8800	
0.01198366	48.0018	9.70061	0	-0.019224483	86.27	2.72	51.5200	86.8100	12.3000	46.0800	
0.01198366	49.0582	9.46073	0	-0.16951561	86.01	1.67	51.3900	86.8700	12.1800	46.2500	
0.00882977	49.0582	9.46073	0	-0.1624454578	85.72	0.73	51.3900	86.4900	12.0500	46.4600	
0.01155953	50.4304	10.3239	0.026607513	-0.333142281	85.56	1.01	51.1000	86.9900	11.9000	46.1000	
0.01110309	50.8309	10.0664	0.021025159	-1.78976059	85.76	1.41	53.6200	87.3000	11.3600	46.3300	
0.01110309	50.8309	10.0664	0.123429298	-0.428965459	85.61	0.88	50.9700	87.0800	11.7600	46.2100	
0.01104998	50.8723	9.69179	0	0.855046055	85.53	1.53	51.2300	86.8800	12.1600	46.7100	
0.01104998	49.9501	8.83252	0.064563751	0.823104044	85.46	1.17	51.3800	87.1100	12.3700	46.9900	
0.00983925	49.9501	13.9139	0.09027916	0.134921074	85.65	2.88	52.2200	86.9400	12.6900	47.1100	
0.01142126	41.5512	10.5115	0.051803537	3.085505999	85.67	2.91	52.4400	87.0200	12.9000	47.4500	
0.01051148	24.6988	1.98186	0.111345551	0.681146387	85.40	4.75	53.4600	87.3000	13.3700	47.5300	
0.01051148	24.6988	1.98186	0.120955997	2.501717992	85.61	5.26	53.6700	87.4900	13.8100	47.6600	
0.01051584	23.1197	1.69556	0	0.139419397	85.14	3.04	54.2800	87.2600	14.1000	47.9400	
0.01051584	23.1197	1.69556	0.13666153	0.183000000	85.02	1.97	54.9500	87.2600	14.4600	48.0500	
0.00983925	27.4413	8.7745	0.137066841	0.823104044	85.31	2.31	54.7300	87.2400	14.7500	48.1600	
0.0105806	22.3895	1.40905	0.051164607	0.464667	85.97	0.46	55.5500	87.3500	15.0800	48.3000	
0.01096659	0.0944024	0.539177	0.07724752	0.14905	85.27	2.47	57.3800	87.2900	15.3400	48.4400	
0.01096659	0.0944024	0.539177	0.34921516	0.0408476	84.88	-0.49	57.5100	87.6300	15.6300	48.6300	
0.01084475	1.09227	0.0408476	0.01680305	0.01680305	85.08	0.95	59.1500	87.4900	15.8900	48.7300	
0.01084475	1.09227	0.0408476	0.01230997	0.01230997	85.05	0.41	60.0600	87.4900	16.3700	48.8900	
0.01055991	3.01269	0.0787002	0	0.150957	84.92	0.95	61.0600	87.5500	16.7600	48.9600	
0.01055991	3.01269	0	0.150957	0.110293435	85.31	1.53	62.0200	87.5700	17.1600	49.0600	
0.01055991	3.01269	0	0.150957	0	0.051164607	85.12	1.68	62.9500	87.6300	17.5500	49.1700
0.01038102	0.01038102	0	0.0944024	0.087163833	84.83	3.40	64.0100	87.6400	17.9700	49.2500	
0.01038102	0	0.0944024	0	0.0944024	84.84	2.64	64.8800	87.6500	18.4300	49.4000	
0.01038102	0	0.0944024	0	0.0944024	84.99	2.58	65.8600	87.6600	18.8600	49.4100	
0.00989732	38.2697	2.88002	0.10840828	0.10840828	84.74	2.57	66.7300	87.6800	19.3600	49.5400	
0.00989732	38.2697	2.88002	0.065588951	0.065588951	84.89	1.14	67.6200	87.7400	19.8800	49.6000	
0.00956603	53.142	5.36086	0	0.115776662	84.69	0.63	68.4100	87.7100	20.4000	49.6300	
0.00956603	53.142	5.36086	0	0.115776662	84.74	1.00	69.1200	87.7400	20.9200	49.6600	
0.00956603	53.142	5.36086	0	0.137431717	84.64	1.38	69.8200	87.7200	21.4900	49.7100	
0.009446491	54.4406	5.33153	0	0.137431717	84.53	0.60	70.4400	87.6900	22.0200	49.6900	

55.5100	24.8100	67.1000	11.0600	57.2000	27.6700	38.1600	71.0200	4.9800	8.7600	72.2400	77.0600	83.9300	7.6800	89.0200	54.5200	33.0300	18.0800
55.6800	24.7100	67.4500	11.2800	57.0700	29.1500	38.2000	71.3900	5.1000	8.9600	72.8500	77.3100	84.6700	7.7000	89.1600	54.4200	32.9300	18.0300
55.8800	24.4400	67.7800	11.5800	57.1300	30.5200	38.0400	71.7300	5.2600	9.0400	73.3300	77.6100	84.3300	7.7800	89.3700	54.3600	32.8400	17.9800
55.9100	24.1400	68.1700	11.9400	57.1100	31.7500	37.7200	71.9700	5.4200	9.0900	73.8000	77.8100	84.2800	7.8200	89.4800	54.2400	32.7100	17.8900
55.9800	24.0000	68.4700	12.3400	57.0800	32.8800	37.6000	72.2700	5.6100	9.0500	74.2800	78.0700	85.2400	8.0000	89.6200	54.1200	32.6500	17.8200
55.9800	24.1400	68.8800	12.8800	57.0500	33.9100	37.8200	72.4900	5.8500	9.1700	74.7200	78.2900	85.7200	8.2000	89.8100	54.0400	32.5500	17.7600
55.9800	24.6500	69.1600	13.6800	57.0800	34.8100	38.4800	72.8000	6.1900	9.3200	75.3400	78.5200	86.4000	8.3700	90.1000	53.9100	32.4500	17.6900
56.0700	25.4800	69.4900	14.9200	57.0100	36.4700	39.5800	73.0500	6.6800	9.5700	75.9500	78.6200	86.8300	8.5700	90.3900	53.8200	32.3100	17.6300
56.0700	25.5800	69.7300	16.5800	56.9800	36.9800	40.9200	73.2800	7.1400	9.9100	76.6200	79.9300	87.5500	10.8100	90.7100	53.8200	32.2800	17.5800
56.0900	27.8200	70.0000	18.6800	56.9800	36.6200	42.4500	73.5000	8.3400	10.3100	77.3300	79.1500	87.9700	12.8200	90.9500	53.6800	32.1800	17.5000
56.1000	29.0500	70.3000	21.1800	56.9800	37.0400	43.9000	73.7100	9.5200	10.7500	77.8400	79.7100	88.3100	14.5000	91.2300	53.5500	32.0700	17.4400
56.1500	30.1200	70.5800	23.8500	57.0000	37.4300	45.1400	73.9400	10.8200	11.2100	78.4400	79.6300	88.8200	16.7600	91.4500	53.5100	31.9800	17.4000
56.2000	30.9300	70.8200	26.6800	56.9800	37.7600	46.0700	74.1800	11.2800	11.7000	78.9300	79.7800	88.8100	18.8300	91.6300	53.4300	31.9100	17.3400
56.1800	31.4300	71.0300	29.7300	56.9400	38.0400	46.6600	74.2800	12.3000	12.7000	79.3100	79.8600	88.8700	20.2400	91.7100	53.2000	31.8000	17.2600
56.1800	31.6800	71.2400	33.1700	57.0000	38.2600	47.0400	74.5000	15.6800	15.8100	79.7900	79.9300	88.9400	21.9800	91.8300	53.2000	31.7100	17.2000
56.2200	31.8300	71.4300	37.0500	57.0100	38.5500	47.3500	74.7200	14.2500	14.7200	79.7300	80.1200	80.2600	18.0900	91.9600	53.1000	31.6400	17.1300
56.2600	32.1300	71.6800	41.7300	56.9800	38.7700	47.7700	74.8900	20.1200	15.8000	80.7100	80.2400	80.9000	22.7200	92.0700	53.0400	31.5600	17.0600
56.3100	32.7200	71.9100	46.9200	57.1500	38.8500	48.4600	74.9800	22.7700	17.7400	81.0500	80.3800	80.9200	23.1200	92.1600	52.9600	31.4300	17.0300
56.2500	32.8000	72.0500	52.1000	57.0000	39.1100	49.4800	75.1600	25.5100	26.1800	81.4300	80.5200	88.9900	24.5500	92.1600	52.8500	31.3300	16.9700
56.0500	35.0200	72.2200	56.8800	57.1600	39.3300	50.8300	75.2400	27.9800	28.0000	81.8000	80.5600	88.8600	25.4400	92.2000	52.7800	31.2200	16.9000
56.3000	36.8100	72.4000	60.9300	57.1900	39.4100	52.2900	75.3100	30.1500	31.000	82.1500	80.6900	88.9700	26.3700	92.2300	52.6700	31.1400	16.8700
56.3500	38.8300	72.6200	64.4000	57.2100	39.5800	53.8900	75.5700	32.0100	32.5000	82.5000	80.6300	89.0000	28.8000	92.3000	52.5800	31.0600	16.7900
56.3100	40.9800	72.7600	67.3000	56.9800	39.7500	55.4800	75.6100	33.9700	33.9800	82.7600	80.2900	89.0500	30.9800	92.4200	52.4900	30.9800	16.7400
56.3500	43.2900	72.8900	69.8000	57.2000	39.8500	56.9300	75.7700	35.2600	38.1000	83.0800	81.5600	89.0400	32.3200	92.1800	52.3900	30.9200	16.7000
56.4200	45.6400	73.1200	71.9400	57.3300	40.1200	58.3100	75.8400	36.6300	42.5600	83.4000	80.9200	89.0800	34.1300	92.3000	52.3100	30.8100	16.6800
56.3400	47.8900	73.1700	73.6900	57.3200	40.1600	59.4400	75.9700	37.8900	46.3900	83.6400	80.7400	88.9300	36.2500	92.2900	52.1600	30.6900	16.5300
56.3800	50.1800	73.4200	75.3300	57.4300	40.2200	60.5100	76.1300	39.0000	51.2800	83.9600	81.0200	89.1000	37.0400	92.2800	52.1500	30.5600	16.4900
56.4000	52.2700	73.5100	76.7200	57.4400	40.4200	61.3600	76.2000	40.1800	45.4800	84.2900	81.2400	88.9000	41.5200	92.2700	52.0300	30.4100	16.4100
56.2800	54.3200	73.5400	77.8400	57.4400	40.33000	61.9400	76.1900	41.2800	59.3500	84.5300	81.3000	88.9300	41.5200	92.1700	51.9100	30.3100	16.3400
56.1700	56.1700	73.7100	78.7800	57.3100	40.2500	62.4600	76.3000	42.2100	62.8800	84.6500	81.2600	89.0200	43.3300	92.1700	51.8200	30.1800	16.2300
56.1800	57.7700	73.5300	79.4300	57.2200	40.0800	62.5600	76.3100	43.1900	66.0000	85.0500	81.0700	88.8000	44.7700	92.0200	51.6800	30.0200	16.0900
56.0000	59.0100	73.8500	79.7500	56.8100	40.5000	63.4400	76.3400	43.3300	67.9700	85.4000	81.4200	88.8000	45.0300	92.0200	51.1900	29.0200	15.2500
55.9100	59.9500	74.5400	80.4600	56.7200	40.4200	64.0200	76.4600	44.8800	72.0200	85.6200	81.5600	88.9100	47.2700	92.0200	50.9000	28.7100	14.3400
55.8800	60.9600	73.5400	80.9700	56.7200	40.4200	64.9100	76.6900	46.2100	74.5500	85.6200	81.4000	88.6800	48.7900	92.1100	50.9000	28.8300	14.2700
55.9400	62.1300	74.0700	81.7600	56.6100	40.9400	65.1300	76.7300	47.2300	76.1600	85.5400	81.5400	88.9400	49.4900	92.1000	51.9600	28.8200	14.2000
55.9400	63.1900	74.2300	82.0600	57.0000	41.2800	65.7200	76.7800	48.1800	77.7000	86.1700	80.8100	89.0000	50.5000	92.0200	51.8800	28.7100	14.1800
56.0300	63.9700	74.4800	82.4700	57.1500	41.5300	66.5300	76.8600	48.9800	78.8400	86.2500	81.6600	89.7500	51.1200	92.0200	51.8800	28.6100	14.1600
56.2100	65.3100	74.5800	82.7600	57.1300	42.1300	66.5700	76.8700	50.1200	80.0500	86.6200	81.9100	88.9900	51.1500	91.9400	51.9400	28.4500	14.0700
56.3000	65.9900	74.7800	83.2100	57.2000	42.0200	66.0100	77.2600	51.0900	81.1700	86.5700	81.9800	88.7000	52.1500	91.8400	51.9100	28.3000	14.0000
56.2900	66.3200	74.7800	83.1400	57.2100	42.4800	66.1600	77.1800	51.9900	81.7800	86.6800	82.0400	88.8900	52.1500	91.8100	50.8200	28.1700	13.9300
56.3000	66.7500	75.0000	83.3500	57.1500	42.5900	66.3800	77.3600	52.8400	82.5000	86.8600	82.1700	88.8700	52.1100	91.8000	50.7000	28.9800	13.8600
56.3600	66.9900	75.0800	83.1300	57.2200	43.0000	66.4400	77.3900	53.1500	86.8100	86.0500	87.3500	52.1100	91.7000	50.7400	28.9500	13.8000	
56.2800	67.3400	75.2800	83.2400	57.1500	44.2800	66.5400	77.4500	54.6000	87.3500	86.9700	87.3100	88.6300	53.1100	91.7100	50.7200	28.8100	13.7200
56.3700	67.5300	75.3800	83.2000	57.2200	44.2800	66.6100	77.6000	55.4600	87.4700	86.9000	87.2900	88.2800	53.1000	91.6400	50.6300	28.7000	13.6500
56.3800	67.6800	75.5200	83.2100	57.2400	44.4200	66.6300	77.7300	56.1200	87.1000	86.5400	87.2100	87.5000	53.0500	91.6400	50.6300	28.6800	13.5800
56.4100	67.9900	75.7100	83.4800	57.3100	44.7200	66.8700	77.8600	57.4400	87.7100	86.7000	87.4700	88.5900	53.1300	91.6700	50.5800	28.6200	13.5100
56.4400	68.1600	75.8000	83.5300	57.3100	44.7700	66.9000	77.9000	58.4100	87.4900	86.4800	87.4300	88.5800	53.1300	91.6700	50.5400	28.5600	13.4400
56.4400	68.5100	76.1100	83.9200	57.3200	44.1000	67.1200	78.1700	60.3800	85.6300	87.3500	87.4700	88.5400	53.1100	91.7300	50.4400	28.4800	13.3700
56.4500	68.7200	76.1900	84.0000	57.3100	44.2800	67.1400	78.2200	61.3400	85.9500	87.3900	87.4700	88.5200	53.1000	91.7400	50.4100	28.4200	13.3000
56.5000	68.8900	76.3500	84.1000	57.3200	44.4500	67.2800	78.3200	62.3400	86.4500	87.4500	87.5400	88.5700	53.0900	91			

8.8000	3.8000	13.000	16.000	7.700	100	34.238096
8.7600	3.8000	15.000	17.000	9.100	100	34.143411
8.7500	3.8100	17.000	11.000	100	100	34.048726
8.7100	3.8000	20.000	18.000	13.000	100	33.818893
8.7000	3.8200	23.000	19.000	15.000	100	33.745734
8.6600	3.8300	25.000	19.000	17.000	100	33.632112
8.6100	3.8500	28.000	20.000	19.000	100	33.499553
8.7000	3.8500	30.000	21.000	21.000	100	33.395331
8.6200	3.8600	32.000	21.000	23.000	100	33.291246
8.5900	3.8800	34.000	22.000	25.000	100	33.13975
8.5600	3.8600	35.000	23.000	27.000	100	33.066128
8.5200	3.8600	37.000	23.000	29.000	100	32.950398
8.5700	3.8900	37.000	24.000	30.000	100	32.836758
8.4900	3.9000	38.000	24.000	32.000	100	32.665262
8.4500	3.8800	38.000	25.000	33.000	100	32.571674
8.3700	3.8900	38.000	25.000	34.000	100	32.439081
8.4000	3.9000	38.000	26.000	35.000	100	32.306522
8.3700	3.8900	38.000	26.000	36.000	100	32.249711
8.3500	3.9100	38.000	27.000	37.000	100	32.13689
8.5800	3.9000	38.000	27.000	38.000	100	32.000553
8.3400	3.8900	38.000	27.000	39.000	100	31.946719
8.3200	3.9000	38.000	27.000	39.000	100	31.795223
8.2900	3.9000	38.000	28.000	39.000	100	31.700538
8.2900	3.8900	37.000	28.000	40.000	100	31.567979
8.2600	3.9000	37.000	28.000	40.000	100	31.43542
8.2300	3.8900	37.000	28.000	40.000	100	31.302861
8.2000	3.8400	37.000	28.000	40.000	100	31.227113
8.1500	3.8400	37.000	28.000	40.000	100	31.075617
8.0900	3.7500	37.000	28.000	40.000	100	30.943058
8.0400	3.6500	37.000	28.000	40.000	100	30.734751
7.8400	3.6200	37.000	28.000	40.000	100	30.499853
7.5600	2.8900	37.000	28.000	40.000	100	28.878925
6.1100	1.5500	37.000	28.000	40.000	100	27.155558
6.3200	6.1100	37.000	28.000	40.000	100	27.951012
6.4200	2.2600	37.000	28.000	40.000	100	28.159319
6.5700	2.2400	37.000	28.000	40.000	100	28.254004
7.0000	2.5300	37.000	28.000	40.000	100	27.932075
6.8700	2.5100	37.000	28.000	40.000	100	28.178556
7.0800	2.7700	37.000	28.000	40.000	100	28.159319
7.1100	2.8900	37.000	28.000	40.000	100	28.197193
7.0700	2.8800	37.000	28.000	40.000	100	28.538059
7.2600	2.9900	37.000	28.000	40.000	100	28.575033
7.1500	2.9200	37.000	28.000	40.000	100	28.424437
7.2600	2.9000	37.000	28.000	40.000	100	28.59487
7.3100	3.1100	37.000	28.000	40.000	100	28.443374
7.3800	3.1400	37.000	28.000	40.000	100	28.197193
7.3200	3.0300	37.000	28.000	40.000	100	28.254004
7.2700	3.0200	37.000	28.000	40.000	100	28.424437
7.3500	3.1200	37.000	28.000	40.000	100	28.291778
7.3200	3.0500	37.000	28.000	40.000	100	28.500185
7.2600	2.9900	37.000	28.000	40.000	100	28.462311
7.3100	3.1000	37.000	28.000	40.000	100	28.59319
7.3400	3.1200	37.000	28.000	40.000	100	28.064534
7.3100	3.1100	37.000	28.000	40.000	100	28.045697
7.3100	3.1300	37.000	28.000	40.000	100	28.026776
7.3300	3.1000	37.000	28.000	40.000	100	27.969949
7.3200	3.0000	37.000	28.000	40.000	100	27.969949

Appendix 4 - Image Quality Model Sample Run

ELECTRONICS/ SUPPORT EQUIP/ DATA COMPRESSION/ OTHER									
OPTICS: USE DIFF LIMITED lens-> NO									
OQF = 1.000	ATMOSPHERIC:								
LENS FILE->	atmos MTF = 1.0000 bit MTF = 1.0000								
FL(mm) = 28.00	ELEC MTF = 1.0000 S. EQPT MTF= 1.0000 D.C. MTF = 1.0000								
wl(um) = 0.65	OTHER MTF = 1.0000 combMTF = 1.0000								
F/# = 5.60									
DETECTOR/FPA:	AIRCRAFT:								
pixel size(um) = 9.000	ALTITUDE(FEET)= 3'000 IN-TRACK AIRCRAFT SPEED(mph)= 100.0 INTEGRATION TIME(SEC)= 0.0167 na								
# of transfers = 2048	IN-TRACK X-TRACK								
phase clocks = 2.000	X-TRACK								
charge transfer = 0.999999	GSD(ft)= 0.9642857 OPT cut off freq (Vo)= 274.725 lp/mm								
	IN-TRK X-TRK								
AT DETECTOR nyquist limit (lp/mm)= 55.55556	image plane size (mm) = 18.432 1/2 angle(deg) = 18.219								
AT TARGET nyquist limit (lp/ft)= 0.51852	IN-TRACK X-TRACK								
theta (deg) = 30.62	DIAGONAL ANGLE= 30.616 (1/2 fld ang)								
AT detector at target	DIAGONAL								
FREQ	radial tang lens MTF @ field angle								
(lp/mm)	diff limited lens MTF @ field angle								
v/Vnqt	OFF-axis lens MTF								
(lp/ft)	on-axis lens MTF								
phi(rad)	FREQ (lp/mm)								
cos(phi)	0.000								
sin(phi)	0.861								
0.00	0.000	1.57	0.00	1.00	0.861	0.637	1.000		0.00
5.00	0.090	0.047	1.55	0.02	1.00	0.841	0.623	0.977	5.00
10.00	0.180	0.093	1.53	0.04	1.00	0.821	0.608	0.954	10.00
15.00	0.270	0.140	1.52	0.05	1.00	0.801	0.593	0.931	15.00
20.00	0.360	0.187	1.50	0.07	1.00	0.781	0.578	0.907	20.00
25.00	0.450	0.233	1.48	0.09	1.00	0.761	0.564	0.884	25.00
30.00	0.540	0.280	1.46	0.11	0.99	0.741	0.549	0.861	30.00
35.00	0.630	0.327	1.44	0.13	0.99	0.721	0.534	0.838	35.00
40.00	0.720	0.373	1.42	0.15	0.99	0.702	0.520	0.815	40.00
45.00	0.810	0.420	1.41	0.16	0.99	0.682	0.505	0.792	45.00
50.00	0.900	0.467	1.39	0.18	0.98	0.662	0.491	0.770	50.00
55.00	0.990	0.513	1.37	0.20	0.98	0.643	0.476	0.747	55.00
60.00	1.080	0.560	1.35	0.22	0.98	0.623	0.462	0.724	60.00
65.00	1.170	0.607	1.33	0.24	0.97	0.604	0.447	0.702	65.00
70.00	1.260	0.653	1.31	0.25	0.97	0.584	0.433	0.679	70.00
75.00	1.350	0.700	1.29	0.27	0.96	0.565	0.419	0.657	75.00
80.00	1.440	0.747	1.28	0.29	0.96	0.546	0.404	0.635	80.00
85.00	1.530	0.793	1.26	0.31	0.95	0.527	0.390	0.612	85.00

MEASURED										DETECTOR/FPA MTF										TOTAL										COMBO									
TOTAL		LENS		FREQ		clockMTF		detectorMTF		x-transMTF		x-TRK		IN-TRK		fpaMTF		fpamTF		total		total		electronic		MTF		BOTH											
OQF	MTF			(lp/mm)	In-TRK		Both																																
1.000	1.000			0.00	1.0000		1.0000			1.0000		1.0000		1.0000		1.0000		1.0000		1.0000		1.0000		1.0000		1.0000		1.0000		1.0000		1.0000		1.0000					
1.000	0.958			5.00	0.9992		0.9967			0.9992		0.9988		0.9950		0.9955																							
1.000	0.909			10.00	0.9967		0.9867			0.9968		0.9952		0.9803		0.9820																							
1.000	0.850			15.00	0.9925		0.9703			0.9931		0.9897		0.9564		0.9603																							
1.000	0.789			20.00	0.9867		0.9475			0.9883		0.9826		0.9240		0.9310																							
1.000	0.724			25.00	0.9793		0.9188			0.9829		0.9745		0.8844		0.8954																							
1.000	0.653			30.00	0.9703		0.8843			0.9772		0.9662		0.8385		0.8544																							
1.000	0.590			35.00	0.9597		0.8446			0.9718		0.9581		0.7877		0.8092																							
1.000	0.525			40.00	0.9475		0.8000			0.9670		0.9511		0.7331		0.7609																							
1.000	0.468			45.00	0.9339		0.7512			0.9633		0.9456		0.6758		0.7104																							
1.000	0.418			50.00	0.9188		0.6986			0.9608		0.9420		0.6168		0.6582																							
1.000	0.375			55.00	0.9022		0.6430			0.9599		0.9406		0.5568		0.6048																							
1.000	0.338			60.00	0.8843		0.5848			0.9605		0.9415		0.4967		0.5506																							
1.000	0.305			65.00	0.8651		0.5248			0.9626		0.9447		0.4371		0.4958																							
1.000	0.279			70.00	0.8446		0.4637			0.9661		0.9498		0.3784		0.4404																							
1.000	0.256			75.00	0.8229		0.4021			0.9707		0.9565		0.3212		0.3846																							
1.000	0.236			80.00	0.8000		0.3406			0.9760		0.9643		0.2660		0.3285																							
1.000	0.220			85.00	0.7761		0.2800			0.9816		0.9727		0.2133		0.2724																							

INTERPOLATION		AIRCRAFT MOTION MTF		IN-TRK		X-TRK	
		LINEAR MOTION SMEAR		smr amt(um)=		0	
interp	interp	IN-TRK		equal pixel amt =		2.53 0.00	
green	red or blue	system		X-TRK		X-TRK	
MTF	MTF	smear MTF		system		smear MTF	
BOTH	BOTH	IN-TRK		X-TRK		X-TRK	
1.0000	1.0000	1.0000		1.0000		1.0000	
0.9901	1.0244	0.9901		0.9787		1.0000	
0.9611	1.0912	0.9611		0.9166		1.0000	
0.9153	1.1830	0.9153		0.8182		1.0000	
0.8564	1.2765	0.8564		0.6910		1.0000	
0.7891	1.3493	0.7891		0.5445		1.0000	
0.7187	1.3867	0.7187		0.3891		1.0000	
0.6507	1.3852	0.6507		0.2358		1.0000	
0.5906	1.3531	0.5906		0.0946		1.0000	
0.5432	1.3074	0.5432		-0.0259		1.0000	
0.5122	1.2678	0.5122		-0.1194		1.0000	
0.5001	1.2502	0.5001		-0.1821		1.0000	
0.5079	1.2615	0.5079		-0.2131		1.0000	
0.5348	1.2974	0.5348		-0.2143		1.0000	
0.5789	1.3434	0.5789		-0.1901		1.0000	
0.6365	1.3802	0.6365		-0.1466		1.0000	
0.7032	1.3896	0.7032		-0.0910		1.0000	
0.7735	1.3610	0.7735		-0.0311		1.0000	

				NDVI			
				background	0.407		
				target	0.775		
				target	1.90418		
				MODtarget=	0.311		
ATMOS MTF						ITM	
		total atmos				ITM	
		atmos MTF	bit MTF	MTF		total sys	total sys
		BOOTH	BOOTH	BOOTH	v(ip/mm)	mtf	mtf
v(ip/cm)					In-TRK	X-TRK	
0.00	1.000	1.000	1.000	1.000	0.00	1.000	1.000
5.00	1.000	1.000	1.000	1.000	5.00	0.292	0.298
10.00	1.000	1.000	1.000	1.000	10.00	0.259	0.283
15.00	1.000	1.000	1.000	1.000	15.00	0.217	0.265
20.00	1.000	1.000	1.000	1.000	20.00	0.170	0.246
25.00	1.000	1.000	1.000	1.000	25.00	0.123	0.225
30.00	1.000	1.000	1.000	1.000	30.00	0.079	0.203
35.00	1.000	1.000	1.000	1.000	35.00	0.043	0.184
40.00	1.000	1.000	1.000	1.000	40.00	0.015	0.163
45.00	1.000	1.000	1.000	1.000	45.00	-0.004	0.146
50.00	1.000	1.000	1.000	1.000	50.00	-0.016	0.130
55.00	1.000	1.000	1.000	1.000	55.00	-0.021	0.117
60.00	1.000	1.000	1.000	1.000	60.00	-0.022	0.105
65.00	1.000	1.000	1.000	1.000	65.00	-0.020	0.095
70.00	1.000	1.000	1.000	1.000	70.00	-0.017	0.087
75.00	1.000	1.000	1.000	1.000	75.00	-0.012	0.080
80.00	1.000	1.000	1.000	1.000	80.00	-0.007	0.073
85.00	1.000	1.000	1.000	1.000	85.00	-0.002	0.068

F56BT(F/5.6,BEST,WITH 650BPFILTER,FLD=-50DEG, RADSCAN)						
freq	input LENS	mtf				
(lp/mm)						
90.00	1.620	0.840				
95.00	1.710	0.887	1.24	0.33	0.94	0.508
100.00	1.800	0.933	1.22	0.35	0.94	0.489
105.00	1.890	0.980	1.20	0.36	0.93	0.471
110.00	1.980	1.027	1.18	0.38	0.92	0.452
115.00	2.070	1.073	1.16	0.40	0.92	0.434
120.00	2.160	1.120	1.14	0.42	0.91	0.416
125.00	2.250	1.167	1.12	0.44	0.90	0.398
			1.10	0.46	0.89	0.380
					0.281	0.441
						0.376
						0.590
						90.00
						95.00
						100.00
						105.00
						110.00
						115.00
						120.00
						125.00

1.000	0.206	90.00	0.7512	0.2209	0.9871	0.9809	0.1638	0.2167	1.000
1.000	0.193	95.00	0.7254	0.1638	0.9921	0.9882	0.1179	0.1619	1.000
1.000	0.181	100.00	0.6986	0.1093	0.9961	0.9942	0.0761	0.1087	1.000
1.000	0.169	105.00	0.6712	0.0579	0.9988	0.9982	0.0388	0.0578	1.000
1.000	0.157	110.00	0.6430	0.0101	1.0000	0.9999	0.0065	0.0101	1.000
1.000	0.146	115.00	0.6142	-0.0337	0.9995	0.9993	-0.0207	-0.0337	1.000
1.000	0.135	120.00	0.5848	-0.0733	0.9975	0.9962	-0.0428	-0.0730	1.000
1.000	0.123	125.00	0.5550	-0.1083	0.9940	0.9911	-0.0597	-0.1073	1.000

0.8420	1.2951	0.8420	0.0259	1.0000
0.9032	1.2045	0.9032	0.0737	1.0000
0.9523	1.1102	0.9523	0.1079	1.0000
0.9852	1.0361	0.9852	0.1258	1.0000
0.9995	1.0012	0.9995	0.1268	1.0000
0.9940	1.0149	0.9940	0.1123	1.0000
0.9691	1.0735	0.9691	0.0853	1.0000
0.9268	1.1616	0.9268	0.0501	1.0000

90.00	1,000	1,000	1,000	1,000	90.00	0.002	0.064
95.00	1,000	1,000	1,000	1,000	95.00	0.004	0.060
100.00	1,000	1,000	1,000	1,000	100.00	0.006	0.056
105.00	1,000	1,000	1,000	1,000	105.00	0.007	0.053
110.00	1,000	1,000	1,000	1,000	110.00	0.006	0.049
115.00	1,000	1,000	1,000	1,000	115.00	0.005	0.045
120.00	1,000	1,000	1,000	1,000	120.00	0.004	0.042
125.00	1,000	1,000	1,000	1,000	125.00	0.002	0.038

Appendix 5 - Image Processing Diagram

CIR Camera Image Processing

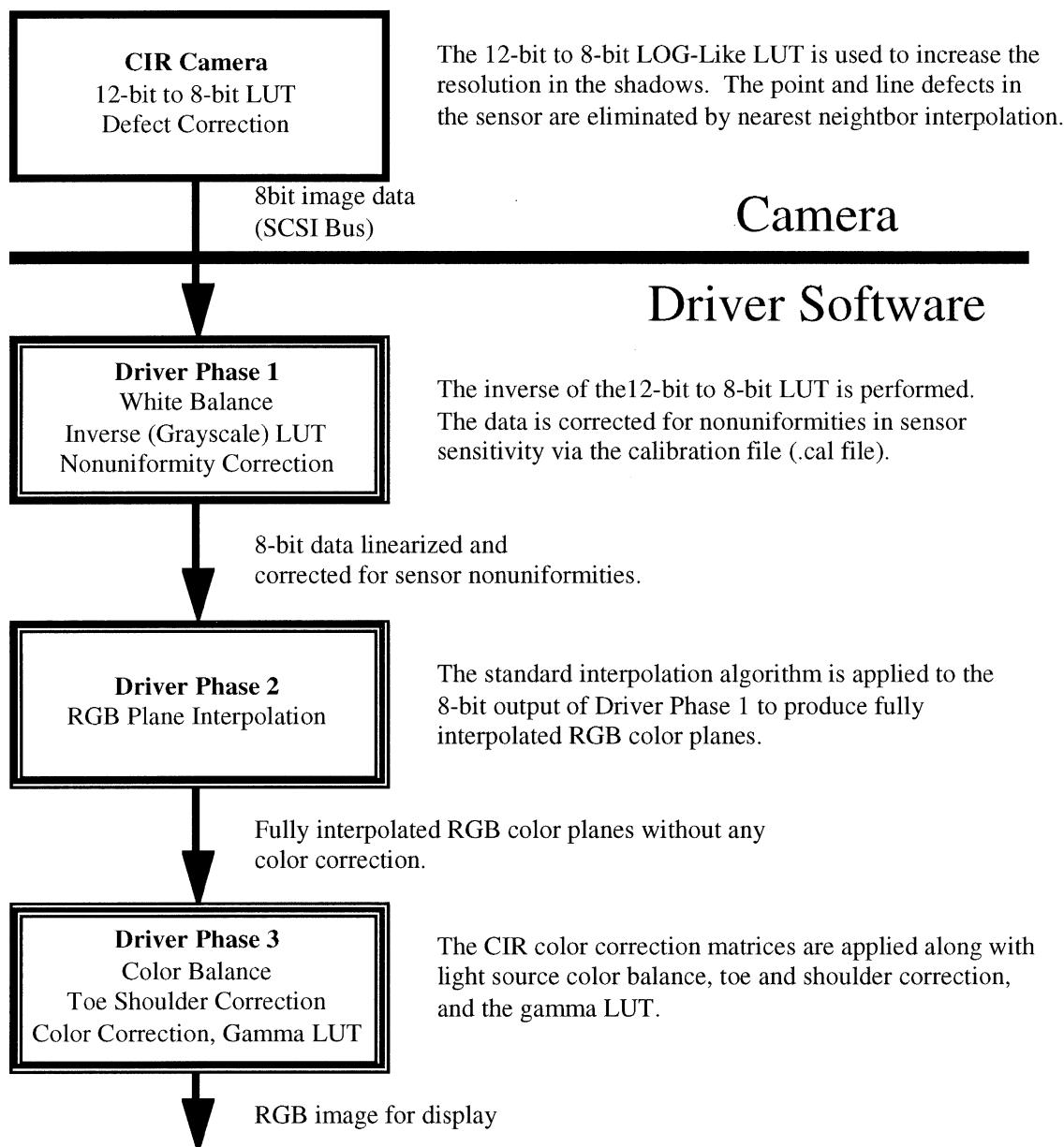


Figure 25: The CIR Camera Image Processing Diagram

7.0 References

1. Adams, J.E. Jr. (1997). *Design of practical color filter array interpolation algorithms for digital cameras*, Eastman Kodak Company, Imaging Research and Advanced Development, Rochester, NY 14653-5408
2. Boyd, R.W. (1983). *Radiometry and the Detection of Optical Radiation*, Wiley, NY.
3. Brainard, K. H. (1994). *Bayesian Method for Reconstructing Color Images from Trichromatic Samples*, Proceedings, IS&T's 47th Annual Conference/ICPS, 375-380
4. Dereniak, E.L. & Crowe, D.G. (1984). *Optical Radiation Detectors*, Wiley, NY.
5. Eastman Kodak Company, *Aerial Data, Kodak Aerochrome II Infrared Film 2443...*, Kodak Pub. AS-69, 12/96
6. Eastman Kodak Company, *Kodak Digital Science Color Infrared Cameras*, Publication : AS-902, 7/97.
7. Eastman Kodak Company, *KAF - 6300 Full-Frame CCD Image Sensor Performance Specification*, Rev. 0 , April 29, 1993.
8. Eastman Kodak Company, *KODAK Professional DCS 420 Digital Camera System - Programmer's Reference Manual* Models: DCS 420m, 420c, September, 1994.
9. Ekiert, S. E., *Threshold Modulation Equation for CCD Imagers*, paper presented at the Optical Society of America, 1979 Annual Meeting, Rochester, NY, 9 - 12 October 1979
10. Gaskill, J.D. (1978). *Linear Systems, Fourier Transforms, and Optics*, Wiley, NY.
11. Goodman, J.W. (1968). *Introduction to Fourier Optics*, McGraw-Hill, NY.
12. Parulski, K.A (1985). *Color Filters and Processing Alternatives for One Chip Camera*, IEEE Trans. Electron Devices, ED-32, 1381-1389
13. Schott, J. R. (1997). *Remote Sensing: The Image Chain Approach*, Oxford, NY.
14. Smith, W.J. (1966). *Modern Optical Engineering*, McGraw-Hill, NY.
15. Tantalo, F.J. (1996). *Modeling the MTF and Noise Characteristics of an Image Chain for a Synthetic Image Generation System*, M.S. Thesis, Rochester Institute of Technology.

